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(54) **Laminated film and process for producing the same**

Verbundfilm und Verfahren zu seiner Herstellung

Film laminé et son procédé de fabrication

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Description

This invention relates to laminated films joined by blocking and a process for producing the same.

As the packaging material used for the packaging bags of photographic photosensitive materials, laminated films consisting of a plurality of film layers are used, and the plurality of the film layers are laminated through an adhesive layer or directly by extrusion laminating. The laminated films are produced through many laminating processes which increase manufacturing cost, and tend to curl. Moreover, tear strength is small.

The inventors disclosed a novel laminated film laminated not by adhesive or extrusion laminating but by blocking in a soft state to a certain degree (USP 4,981,734, EP 0,369,447A). The laminated films laminated by blocking have a great tear strength, Gelbo test strength and impact puncture strength, and curling does not occur. However, the pseudo-adhesion by blocking is unstable, and laminated films were occasionally separated from a cut end in a low temperature season. The pseudo-adhesion was also occasionally separated partially in the laminating process of other flexible sheets or in the bag-making process, resulting in the occurrence of wrinkling, furrowing or blistering troubles. These troubles became a problem in winter and in strongly air cooled rooms.

The object of the invention is to provide a laminated film laminated by blocking in a suitable strength which does not separate, for example, during the laminating process and the bag-making process, irrespective of seasons, when it is produced in the normal conditions; wherein the pseudo-adhesion does not vary caused by film thickness and temperature variation e.g. due to seasons or cooling efficiency by air; and a process for producing the same.

The present invention provides laminated films and processes for producing them which have achieved the above objects.

Thus, the present invention provides:

A laminated film comprising two thermoplastic resin films, the inner surfaces of which are joined by blocking, said film having strongly joined portions and weakly joined portions, wherein the peeling strength of the strongly joined portions is at least twice that of the weakly joined portions; and

a process for producing the above laminated film which comprises

pressing two thermoplastic resin films by an embossing roll or

flat-pressing a tubular film molded by an inflation process, by a pressure roll into flat to join the inner surfaces by blocking, and cutting by fusion.

The process for producing a laminated film preferably comprises heating the surface of a tubular film molded by an inflation process, and then pressing the tubular film by a pressure roll into flat to join the inner surfaces by blocking.

The laminated film preferably comprises a coextruded multilayer inflation film, the inner surfaces of which are joined by blocking, wherein the Shore hardness (ASTM D-2240) of the inner layer comprising the thermoplastic resin is lower than that of the outer layer comprising the thermoplastic resin.

The laminated film preferably comprises a coextruded multilayer inflation film, the inner surfaces of which are joined by blocking, wherein the inner layer comprises an acid-modified polyolefin resin.

In the laminated film which is laminated by blocking, the end portions are preferably joined more strongly than the central portion.

The process for producing the above laminated film preferably comprises pressing a film laminated by blocking in a linear form with a prescribed width, and then cutting the pressed portion. Preferably, the cut end of the film is thickened.

The laminated film of the invention may contain a light-shielding material in at least two layers.

In the following the drawings are briefly described.

Figures 1 through 15 are partially sectional views of a laminated film embodying the invention.

Figure 16 is a sectional view illustrating a coextruded double layer film which is deflated and of which the inner layer is joined by blocking.

Figures 17 through 21 are partial plan views illustrating various patterns of the strongly joined portions and the weakly joined portions.

Figures 22 through 28 are partially sectional views of a laminated film of the invention, wherein the end portions are joined more than the central portion.

Figure 29 is a schematic illustration of an inflation film molding apparatus showing the state of producing a laminated film laminated by blocking.

Figure 30 is a perspective view illustrating the manufacturing state of the laminated film of the invention wherein the cut end is joined by heat fusion.

Figure 31 is a partially sectional view of the laminated film of the invention produced by the apparatus of Figure 30.

Figure 32 is a schematic side view of an apparatus for producing the laminated film of the invention having a pattern of the strongly joined portions.

Figure 33 is a schematic plan view of another apparatus for producing the laminated film of the invention having a pattern of the strongly joined portions.

5 Figure 34 is a perspective view illustrating the manufacturing of the laminated film of the invention, the end portions of which are joined more strongly than the central portion.

Figure 35 is a perspective view of a slitting apparatus applicable to the invention, and Figure 36 is a partially sectional view of an inflation film slitted by this apparatus.

Figure 37 is a schematic side view of a slitting apparatus also applicable to the invention.

10 In the following the invention is described in more detail.

To join by blocking means that the deflated (in the specification, "deflated" means "rendered flat by passing a pressure roll") inner surface of an inflation film is joined without using an adhesive and heat fusion.

The blocking is, for example allowed to occur by passing the nip roll of an inflation film molding machine with weakening cooling conditions, or by passing a pressure roll composed of a heating metal roll and an elastic roll, such as a heat-resistant rubber roll or a cotton roll, before the film is not entirely cooled. The pressing form includes the entire face pressing, spot pressing, pressing in longitudinal streaks, pressing in lattice pattern, pressing in lateral streaks, pressing in other embossed patterns. The metal roll may be flat or provided with various embossing, such as spots, streaks, lattice, cloth mark, or other embossed patterns; e.g., more than 210 patterns are disclosed in "BEALON SHIBO (Crimp)" (published by NGK Bealon Corp. Ltd.)

20 It is preferred to heat the tubular film before blocking by the nip roll or pressure roll. When the inner surface of the inflation film is heated, it can be conducted by heating the mandrel. When the outer surface of the inflation film is heated, it can for example be conducted by using a far-infrared heater in a ring form, blowing hot air, using nichrome wire heaters in a ring form or using a heating bar in a ring form. The above heaters may be composed of a plurality of commercial linear heaters. A preferred heating temperature renders the inner surface of the inflation film to around the softening point, in view of not degrading the appearance of the film outer surface and obtaining a suitable adhesion strength by blocking. The heating temperature, therefore, for example depends on the film molding speed, film thickness and the resin composition. For example, in the case that the inner surface is composed of a L-LDPE resin, the heating is conducted so that the temperature of the inner surface becomes more than 40°C, preferably 50 to 140°C, more preferably 60 to 120°C.

30 The inflation film may either be a single layer film or a multilayer film. In the case of a single layer film, it is necessary to provide a temperature difference between the inner surface and the outer surface. The temperature difference may be formed at the ring die or by air-cooling of the outer surface alone.

It is preferred to provide strongly joined portions and weakly joined portions in the joined portion by blocking. The peeling strength of the strongly joined portions is not less than twice, preferably not less than three times, particularly preferably not less than five times, that of the weakly joined portions. When the peel strength of the strongly joined portions is less than twice that of the weakly joined portions, there is not only a possibility that the pseudo-adhesion does not occur at the weakly joined portions in winter and strongly air-cooled room, but also the pseudo-adhesion at the strongly joined portions reduces. As a result, the separation at the pseudo-adhesion and wrinkling occur in the laminating process of other flexible sheets or in the bag-making process. In order to induce none of the above problems, to improve physical strength, such as tear strength, to prevent curling and to improve flexibility, a suitable peel strength of the strongly joined portion is 2 to 250 g/15 mm width, preferably not more than 100 g/15 mm width, more preferably not more than 50 g/15 mm width. When the peel strength is more than 200 g/15 mm width, at the strongly joined portions, the inner surfaces are joined substantially in a heat fusion state, and the laminated film tends to tear at the boundary between the strongly joined portions and the weakly joined portions. Moreover, at the strongly joined portions, flexibility and Gelbo test strength decreases, and pinholes tend to occur. When the peel strength is less than 2 g/15 mm width, the portions joined by blocking tend to be separated similar to the conventional laminated films laminated by blocking. A suitable peel strength of the weakly joined portions is not more than 150 g/15 mm width, preferably not more than 50/15 mm width, more preferably not more than 20 g/15 mm width. The lower limit is 0.01 g/15 mm width, preferably 0.1 g/15 mm width. A suitable interval between the strongly joined portions and weakly joined portions is 1 to 100 mm, preferably 2 to 50 mm. When the interval is less than 1 mm, the laminated film is similar to that entirely laminated by the strongly joined portions. As a result, to ensure flexibility and physical strength of the laminated film is difficult, and wrinkling and streaks tend to occur. When the interval exceeds 100 mm, the laminated film is similar to that entirely laminated by the weakly joined portions, and similar problems to the conventional laminated films laminated by blocking occur. The form of the strongly joined portions may e.g. be spots, streaks or lattice.

55 The strongly joined portions may be provided at the end portions to form a laminated film wherein the end portions are joined more strongly than the central portion. For example in the case of a rectangular film, it is not necessary that the end portions to be joined by the strongly joined portions are on all four ends, and it is sufficient to join at least two parallel sides by the strongly joined portions. Besides, if one end is a folded end, it is sufficient to join the other end in parallel to the folded end by strongly joined portions. The peel strength of the strongly joined portions is preferably not

less than 20 g/15 mm width, more preferably not less than 50 g/15 mm width, particularly not less than 150 g/15 mm width. The peel strength of the weakly joined portions is preferably not more than 150 g/15 mm width, more preferably not more than 50 g/15 mm width, particularly preferably not more than 20 g/15 mm width.

The strongly joined portions and weakly joined portions can be formed by the method of indenting the inner surface and/or outer surface of a single layer or multilayer inflation film, e.g. by processing the ring die and then pressing by a smooth surface pressure roll; the method of using a cooling apparatus having ribs at constant intervals in the longitudinal direction, and pressing by a pressure roll having ribs at constant intervals in the lateral direction (see Example 13); the method of using an embossing roll as the nip roll of a single layer or multilayer inflation film molding machine; the method of joining the inner surface of the deflated single layer or multilayer inflation film entirely by the weakly joined portions by passing a nip roll, and then forming indentations by passing an embossing roll provided behind the nip roll to form the strongly joined portions (see Examples 11 and 12). A preferred method comprises joining the inner surface of the deflated single layer or multilayer inflation film by blocking, heating the film laminated by blocking by a heater, such as a hot air heater or a far-infrared heater, and then pressing by an embossing roll. The heating temperature by the heater is lower than the melting point, preferably softening point, of the inflation film. When the heating temperature exceeds the melting point, not only the flatness of the inflation film is degraded, but the outer surface layers faced each other formed by winding the inflation film are also joined by blocking. As a result, unwinding of the roll of the inflation film is difficult, and breakage of the inflation film occurs.

In the laminated film of the invention, wherein the end portions are joined more strongly than the central portion, the strongly joined portions can be formed by pressing by a pressure roll or a heating roll, and the strength of the strongly joined portions is controlled, e.g., by adjusting pressure and/or temperature. Cutting of the strongly joined portions may be conducted before or after the formation of the strongly joined portions. For example, a laminated film laminated by blocking is pressed in a linear form with a prescribed width by a pressure roll to form the strongly joined portions, and then the strongly joined portions are cut to obtain a laminated film having the strongly joined portions at ends. The laminated film by blocking is preferably produced from an inflation film by deflating, but may be produced by superimposing two films separately molded and then joining by blocking. The separately molded films may be identical with or different from each other in resin composition, molding method, such as inflation process, T die method or casting method, thickness, color and layer construction. When packaging bags are made of the above laminated film, the strongly joined portions are preferably utilized as the sealing end.

As the method for joining the cut end of the laminated film by heat fusion, e.g. the laser beam cutting, the ultrasonic cutting, the flame cutting, the electric discharge cutting, the heated rotary blade cutting or the heated razor blade cutting are usable. Among them, the heated razor blade cutting is preferred, in view of inexpensive equipment costs and the ease of width change. A suitable temperature is around the Vicat softening point (ASTM D-1525) of the inner layer, actually ranging from 50°C to the melting point, preferably from 70 to 150°C, more preferably from 80 to 120°C.

Heretofore, the edge trimming and slitting into a prescribed width of a continuously traveling film web are conducted by slitting the film by a fixed blade at a free traveling portion between conveying rollers, slitting by a combination of a fixed blade and a rotary blade (e.g. Japanese Patent KOKAI No. 64-58492), slitting by a combination of a rotating roll with channels and fixed blades, slitting by a traveling rotary blade which travels with rotating along a fixed blade, slitting by laser beam.

The slitting by the fixed blade is cheap and excellent in workability. However, in the case of elevating the traveling speed of the film or slitting a flexible polyolefin resin film containing carbon black which has a great tear strength and elongation, various troubles occur, such as wrinkling at the free traveling portion, difficulty in slitting or breakage of the film. Particularly, when the film to be slitted is used for a laminated film, unless incision is good, it causes to break the web. Besides, in the case of slitting a film composed of a linear low density polyethylene (L-LDPE) resin containing carbon black, which is flexible, great in tear strength in the longitudinal direction and liable to elongate, for a long period, the contact portion of the fixed blade with the film is locally heated, resulting in the reduction of sharpness of the blade. Therefore, it is necessary to change the blade about every two days. The generation of cuttings in quantity is also a problem. The cuttings and dust suspended in air adhere to the film, and are entrained into the film roll. As a result, they induce indentations or projections by pressing film layers, or remain fixed to the film.

The slitting by the combination of a fixed blade and a rotary blade is excellent in good incision of e.g. photographic films and magnetic tape films and a small quantity of cuttings. However, the apparatus is expensive and requires a lot of time for registering the upper blade and the lower blade. Moreover, it is not suitable for slitting various films made of various resins which are cheap and different in thickness and molecular orientation, such as packaging films, particularly the films being flexible, great in tear strength and liable to elongate, such as polyolefin resin films containing carbon black.

The slitting by a combination of a rotating roll with channels and fixed blades is preferred in a wide utilization because of cutting with stretching in the width direction on the surface of the roll with channels. However, the life of the blade is short similar to the above fixed blade, and it is necessary to change the blade about every two days while the film molding line is stopped. Moreover, a cleaning means of cuttings is necessary, because cuttings are generated.

The slitting by a traveling rotary blade is for example applicable for cutting or slitting papers in a limited length, but

it is impractical for slitting a traveling film web.

The slitting by laser beam is for example restricted in utilization in view of the manufacturing speed, cost, maintenance and safety, although the generation of cuttings is prevented.

However, the aforementioned heated razor blade cutting is excellent, particularly in slitting a film being flexible, great in tear strength and liable to elongate, such as a polyolefin resin film containing carbon black, due to e.g. rare production of cuttings, long life of blade, high productivity, incision with a high strength and rare breakage of slit polyolefin resin film. The heated razor blade cutting is also applicable to various films not laminated by blocking. The incision slit by the heated razor blade is thickened compared with before slitting.

The inflation film of which the inner surface is joined by blocking may be a single layer film or a coextruded multilayer film. In the case of a single layer film, preferred resins composing the film are those suitable for the inner layer of the coextruded multilayer film.

Preferable inflation films are coextruded multilayer films wherein the resin composing the inner layer which is joined by blocking is different from the resin composing the outer layer wherein blocking does not occur. Preferred resins used for the inner layer are, for example ethylene copolymer resins, propylene copolymer resins, thermoplastic resin elastomers, such as ethylene-propylene copolymer rubber and ethylene-propylene-diene ternary copolymer rubber, thermoplastic resins containing a tackifier and modified polyolefin resins (acid-modified polyolefin resins), having a low softening point and excellent physical strength. The thermoplastic resins containing a low polymerization degree polyolefin resin having a mean molecular weight of 300 to 7,000 and the thermoplastic resins containing a tackifier, such as rosin resins, terphenol resins, petroleum resins, cumarone-indene resins, styrene resins and phenol resins, are preferable in order to ensure pseudo-adhesion by blocking. It is preferred that the inner layer contains at least one of the above resins in an amount of more than 50 wt. % in total of the above resins. Particularly preferred resins are polyolefin resins containing more than 50 wt. % in total of the ethylene- α -olefin copolymer resin and/or ethylene-vinyl acetate copolymer resin having a Vicat softening point lower than the outer layer by 5°C or more, because of obtaining a laminated film stable in pseudo-adhesion by blocking and excellent in physical strength. Other suitable resins include low density homopolyethylene resin and medium - high density homopolyethylene resin.

Suitable ethylene copolymer resins are, for example, ethylene-vinyl acetate copolymer resins, ethylene-propylene copolymer resins, ethylene-1-butene copolymer resins, ethylene-butadiene copolymer resins, ethylene-vinyl chloride copolymer resins, ethylene-methylmethacrylate copolymer resins, ethylene-methyl acrylate copolymer resins, ethylene-ethyl acrylate copolymer (EEA) resins, ethylene-acrylonitrile copolymer resins, ethylene-acrylic acid copolymer resins, ionomer resins (copolymers of ethylene and unsaturated acids crosslinked using metals, such as zinc), ethylene- α -olefin copolymer (L-LDPE) resins and ethylene-propylene-butene-1 ternary copolymer resins. Among the above ethylene copolymer resins, L-LDPE resins and EEA resins are preferred, because they are excellent in film moldability and heat sealing properties and are great in bag rupture strength, impact puncture strength and tear strength. L-LDPE resins are particularly preferred.

In order to adjust the properties to be necessary, it is preferred to blend with other thermoplastic resins, elastomers, rubbers, various additives or modifiers.

The L-LDPE resin is called third polyethylene resin, and it is a low cost high strength resin, having the advantages of both low, medium density polyethylene resin and high density polyethylene resin, which meets the requirements, i.e. resource conservation and energy conservation, of the times. The L-LDPE resin is a copolymer of ethylene and α -olefin, and it has a linear structure having short branches. The number of carbon atoms of the α -olefin is 3 to 13. Preferably, the α -olefin has a number of carbon atoms of 4 to 10, and examples of the α -olefin are butene-1, 4-methylpentene-1, hexene-1, heptene-1 and octene-1. The density is usually in the range of 0.87 to 0.95 g/cm³, and the melt index is usually 0.1 to 50 g/10 minutes. Most of the L-LDPE resins are synthesized by a low pressure method, and partly they are synthesized by a modified high pressure method. Examples of commercial L-LDPE resins are "G-Resin" and "TUFLIN" and "NUC-FLX" (UCC), "NUC Polyethylene-LL" and "TUFTHENE" (Nippon Unicar) "Excelene VL" (Sumitomo Chemical), "Idemitsu Polyethylene-L" and "Moretec" (Idemitsu Petrochemical), "Dowlex" (Dow chemical), "Suclear" (Dupont de Nemour, Canada), "Marlex" (Phillips), "Neozex" and "Ultex" (Mitsui Petrochemical Industries), "Nisseki Linirex" (Nippon Petrochemicals), "Mitsubishi Polyethylene-LL" (Mitsubishi Petrochemical) and "Stamilex" (DSM) (all trade names). Preferable L-LDPE resins are copolymers of ethylene and α -olefins of which the number of carbon atoms is 6 to 8, having a melt index (MI) of 0.8 to 10 g/10 minutes (ASTM D-1238) and a density of 0.870 to 0.940 g/cm³ (ASTM D-1505), manufactured by a liquid process or a vapor process. Very low density L-LDPE resins having a density of less than 0.910 g/cm³ are also preferred.

The EEA resins are not restricted, and commercial EEA resins have, for example, a comonomer content of 7 to 41 %, a MI of 1.5 to 1500 g/10 minutes (ASTM D-1238), a density of 0.93 to 0.95 g/cm³ (ASTM D-1505), a brittle temperature of -40°C to less than -75°C (ASTM D-746) and a tensile strength of 14 to 160 kg/cm² (ASTM D-638).

A preferable coextruded multilayer inflation film has an inner layer containing a thermoplastic resin having a Shore hardness (ASTM D-2240) lower than the thermoplastic resin of the outer layer. A suitable Shore hardness of the thermoplastic resin having a lower Shore hardness contained in the inner layer is lower than 60 D, preferably 10 to 50 D in view of ensuring pseudo-adhesion by blocking, flexibility and Gelbo test strength. The Shore hardness is preferably

lower than that of the thermoplastic resin of the outer layer by 2 D or more, particularly 5 D or more. Suitable thermoplastic resins for the inner layer are polyolefin copolymer resins, such as acid-modified polyolefin resins, L-LDPE resins, EEA resins and EVA resins.

Another preferable coextruded multilayer inflation film has an inner layer containing an acid-modified polyolefin resin.

The acid-modified polyolefin resin is a modified polyolefin resin which is modified by grafting an unsaturated carboxylic acid compound, and includes graft-modified polyethylene resins, graft-modified polypropylene resins, graft-modified ethylene copolymer resins and graft-modified poly- α -olefin resins, such as graft-modified ethylene-ethylacrylate copolymer resins, graft-modified ethylene-vinyl acetate copolymer resins, graft-modified polybutene-1 resins and graft-modified poly-4-methylpentene-1 resins. A preferred grafting rate is 0.01 to 10 %.

The unsaturated carboxylic acid compound usable as the modifier of the polyolefin resin is for example acrylic acid, methacrylic acid, crotonic acid, isocrotonic acid, fumaric acid, maleic acid, itaconic acid, citraconic acid, angelic acid, tetrahydrophthalic acid, sorbic acid, mesaconic acid, end-cis-bicyclo[2,2,1]-hepto-5-en-2,3-dicarboxylic acid, maleic anhydride, itaconic anhydride, citraconic anhydride, aconitic anhydride, methyl acrylate, methyl methacrylate, ethyl methacrylate, ethyl acrylate, n-butyl acrylate, glycidyl acrylate, glycidyl methacrylate, glycidyl maleate n-butyl methacrylate, maleic acid monoethyl ester, maleic acid diethyl ester, fumaric acid monomethyl ester, fumaric acid dimethyl ester, itaconic acid diethyl ester, acrylamide, methacrylamide, maleic acid monoamide, maleic acid diamide, maleic acid-N-monoethylamide, maleic acid-N,N-diethylamide, maleic acid-N-monobutylamide, maleic acid-N,N-dibutylamide, fumaric acid monoamide, fumaric acid diamide, fumaric acid-N-monoethylamide, fumaric acid-N,N-diethylamide, fumaric acid-N-monobutylamide, fumaric acid-N,N-dibutylamide maleimide, N-butylmaleimide, N-phenylmaleimide, malonyl chloride, monomethylmaleate, dimethylmaleate, dipropylmaleate, potassium acrylate, sodium acrylate, zinc acrylate, magnesium acrylate, calcium acrylate, sodium methacrylate or potassium methacrylate. Two or more unsaturated carboxylic acid compounds may be combined. Preferable unsaturated carboxylic acid compounds are acrylic acid, maleic acid and maleic anhydride. Maleic anhydride is particularly preferred. A suitable amount of the unsaturated carboxylic acid compound is 0.01 to 20 parts by weight, preferably 0.2 to 5 parts by weight, per 100 parts by weight of the polyolefin resin base in view of securing adhesive strength.

The grafting modification method may be any known method, such as the method of reacting in a melted state disclosed in Japanese Patent KOKOKU No. 43-27421; the method of reacting in a solution state disclosed in Japanese Patent KOKOKU No. 44-15422; the method of reacting in a slurry state disclosed in Japanese Patent KOKOKU No. 43-18144; and the method of reacting in a vapor state disclosed in Japanese Patent KOKOKU No. 50-77493. Among them, the melting method using an extruder is preferred because of simple operation and inexpensiveness.

A peroxide is added in order to accelerate the reaction between the polyolefin base resin and the unsaturated carboxylic acid. Suitable peroxides are organic peroxides, such as benzoyl peroxide, lauroyl peroxide, dicumyl peroxide, α,α' -bis(t-butylperoxydiisopropyl)benzene, 2,5-dimethyl-2,5-di(t-butylperoxy)hexane, 2,5-dimethyl-2,5-di(t-butylperoxy)hexyne, di-t-butyl peroxide, cumene hydroperoxide, t-butyl-hydroperoxide, t-butylperoxylaurate, t-butylperoxybenzoate, 1,3-bis(t-butylperoxyisopropyl) benzene, di-t-butyl-diperoxyphthalate, t-butylperoxymaleic acid and isopropyl percarbonate; azo compounds, such as azobisisobutyronitrile; and inorganic peroxides such as ammonium persulfate. Two or more peroxides may be combined. Suitable peroxides are di-t-butylperoxide, dicumylperoxide, 2,5-dimethyl-2,5-di(t-butylperoxy)hexane, 2,5-dimethyl-2,5-di(t-butylperoxy)hexyne and 1,3-bis(t-butylperoxyisopropyl) benzene, having a decomposition temperature between 170°C and 200°C. A suitable amount of the peroxide is 0.005 to 5 parts by weight, preferably 0.01 to 1 part by weight per 100 parts by weight of the polyolefin resin base.

There are commercial acid-modified polyolefin resins, such as "N polymer" (Nippon Petrochemicals), "Admer" (Mitsui Petrochemical Industries), "ER Resin" (Showa Denko), "Novatec-AP" (Mitsubishi Chemical Industries), "Modic" (Mitsubishi Petrochemical) and "NUC-Ace" (Nippon Unicar) (all tradenames).

The unmodified polyolefin resin is e.g. a polyethylene resin, polypropylene resin, ethylene copolymer resin or polyvinyl chloride resin.

A suitable content of the acid-modified polyolefin resin in the inner layer is 5 to 80 wt. %, preferably 10 to 60 wt. %. When the content is less than 5 wt. %, it is difficult to always form the pseudo-adhesion by blocking over the whole inner surface. Moreover, the effect upon the improvement in the dispersibility of light-shielding material reduces. In the case of using polyester resins, polyamide resins or ethylene-vinyl alcohol copolymer resins, layer separation occurs at the boundary between the inner layer and the outer layer. When the content exceeds 80 wt. %, although no problem occurs in the pseudo-adhesion by blocking over the whole surface and in the improvement in the dispersibility of light-shielding material, the acid-modified polyolefin adversely affects photographic photosensitive materials. Scrubbability of the mold is also degraded.

The resin contained in the inner layer may be other than the acid-modified polyolefin. Although there are various resins blendable with the acid-modified resin, such as various thermoplastic resins, various elastomers and tackifier resins, polyolefin resins, such as various ethylene copolymer resins, various propylene copolymer resins, homopolyethylene resin and homopolyethylene resin, which are inexpensive and excellent in film moldability, are preferred. Particularly preferred resins are L-LDPE resins, EEA resins, EVA resins and LDPE resins. Both of the Shore hardness and

Vicat softening point of the resins are preferably lower.

As the resin used for the outer layer, for example various thermoplastic resins and various elastomers, are usable, and it is necessary to select those resin having a higher antiblocking ability, wear resistance, Shore hardness and Vicat softening point than the inner layer. Moreover, in the case of heat sealed uses, such as laminated films for bags, heat sealability is necessary, and in the case of the use for photographic photosensitive materials, it is necessary to select a resin not affecting the photographic properties adversely. In the case of requiring heat sealability, suitable resins for the outer layer are various polyolefin resins having a Shore hardness and Vicat softening point higher than the inner layer, and in the case of not requiring heat sealability, suitable resins are various polyamide resins, various polyester resins, high molecular weight polyethylene resins and high molecular weight polypropylene resins.

Preferable resins for the outer layer are those having a Vicat softening point higher than the inner layer by 5°C or more, preferably 10°C or more, and being excellent in inflation film moldability, physical strength and heat sealing properties (e.g. appearance, prevention of pinholes and rupture, prevention of the decrease in strength). Such a resin includes an ethylene- α -olefin copolymer resin having a density of more than 0.920 g/cm³, a homopolyethylene resin having a density of more than 0.920 g/cm³, a homopolypropylene resin, a propylene- α -olefin copolymer resin, a polyamide resin, such as nylon 6, nylon 66, nylon 11 and nylon 12, including a copolymer resin with another resin, a polyester resin and a ethylene-vinyl alcohol copolymer resin. The resin used in the outer layer is preferably the above resin alone or a resin blend containing more than 50 wt. % of the above resin. Particularly preferable resins are homopolyethylene resins and ethylene- α -olefin copolymer resins having a density of more than 0.920 g/cm³, polyamide resins and polyester resins. In view of heat sealing properties, preferable resins are α -olefin copolymer resins having a number of carbon atoms of 2 to 6, more preferably ethylene- α -olefin copolymer resins, particularly preferably copolymer resins and α -olefin resins having a number of carbon atoms of 4 to 10. A suitable content of these resins is more than 3 wt. %, preferably more than 10 wt. %, more preferably more than 15 wt. %, in view of ensuring heat sealing strength with time. By composing the outer layer of an inflation film of a resin composition containing more than 15 wt. % of an ethylene- α -olefin copolymer resin, heat sealing strength with time of packaging bags is ensured, and hot tack properties and physical strength are rendered excellent.

The Shore hardness of the resin used for the outer layer is higher than the inner layer, and higher than 50 D, preferably higher than 60 D, particularly preferably higher than 70 D.

The inflation film may preferably contain carbon black, metal powders (including pastes), carbon fibres, conductive polymers, metal fibers, antistatic agents, and/or lubricants in order to improve the antistatic properties.

Carbon black, which is the most preferable as the light-shielding material, is divided into gas black, oil furnace black, channel black, anthracene black, acetylene black, Ketchen carbon black, thermal black, lamp black, vegetable black and animal black according to its origin. Among these, oil furnace carbon black is preferable in terms of light-shielding character, costs and improvement of properties. On the other hand, since acetylene black and Ketschen carbon black have antistatic characteristics, they are also preferable, though they are expensive. They may be blended to the oil furnace black in order to improve its characteristics. Though, there are various blending methods, such as dry coloring, liquid coloring, paste color, masterbatch methods using pellets, compound color pellets and granular color pellets, the masterbatch method using masterbatch pellets is preferred in view of costs and less contamination of the working place. Japanese Patent KOKOKU No. 40-26196 discloses a method of making a masterbatch of polymer-carbon black by dissolving the polymer in an organic solvent and dispersing the carbon black into the solution. Japanese Patent KOKOKU NO. 43-10362 discloses another method of making a masterbatch by dispersing the carbon black into polyethylene. The inventor also disclosed a resin composition for color masterbatch (EP 0,277,598A).

Particularly preferable carbon black for the packaging material for photographic photosensitive materials is the oil furnace carbon black having a pH of 6 to 9, a mean particle size of 10 to 120nm (m μ) a volatile components content of less than 2 %, a content of cyanides and sulfur components of less than 1.0 %, preferably less than 0.5 %, particularly preferably less than 0.1 %, and an oil absorption value of more than 50 ml/100 g in view of no occurrence of fogging, rare occurrence of photosensitivity deviation and great light-shielding ability. Moreover, when it is blended with L-LDPE resin, the lumps of carbon black and fish eyes rarely occur. Channel black is not preferred because it contains components inducing fogging, such as sulfur components, in quantity and is expensive.

Metal powders include e.g. iron powder, stainless steel powder, copper powder, lead powder and aluminum powder. Carbon fibers include silicon carbide fibers, as well as pure carbon fibers. Carbon fibers improve the conductivity and the physical properties, but they are expensive. Metal fibers are, e.g. brass fibers and stainless steel fiber. Metal fibers improve the conductivity, but they are expensive and increase the specific gravity.

In any event, in the case of using the laminated film of the invention in packaging materials for photosensitive materials, particularly on the photosensitive material side of the packaging material, it is preferred to select a light-shielding material having a total content of cyanides and sulfur components of less than 1 %, preferably less than 0.5 %, more preferably less than 0.1 %, in order not to degrade the photographic properties, such as fogging, sensitivity, tone and color balance. Examples of the light-shielding materials usable in the present invention are described below.

Oxides ...e.g. silica, diatomaceous earth, alumina, titanium dioxide, iron oxide, zinc oxide, magnesium oxide, anti-

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many oxide, barium ferrite, strontium ferrite, beryllium oxide, pumice, pumice balloon, alumina fiber;

Hydroxides ...e.g. aluminum hydroxide, magnesium hydroxide, basic magnesium carbonate;

Carbonates ...e.g. calcium carbonate, magnesium carbonate, dolomite;

Sulfates, sulfites ...e.g. calcium sulfate, barium sulfate, ammonium sulfate, calcium sulfite;

Silicates ...e.g. talc, clay, mica, asbestos, glass fiber, glass balloon, glass bead, calcium silicate, montmorillonite, bentonite;

Carbons ...e.g. carbon black, graphite, carbon fiber, carbon hollow bead;

Others ...e.g. iron powder, copper powder, lead powder, aluminum powder, molybdenum sulfide, boron fiber, silicon carbide fiber, brass fiber, potassium titanate, lead titanate zirconate, zinc borate, barium metaborate, calcium borate, sodium borate, aluminum paste;

Organic Compounds:

e.g. wood flour, such as pine, oak and sawdust, husk fibers, such as almond, peanut and chaff, cotton, jute, paper pieces, cellophane pieces, nylon fibers, polypropylene fibers, starch, aromatic polyamide fibers.

Among them, preferred absorbents make the material opaque. Light-absorptive carbon black, titanium nitride and graphite are particularly preferred because they are excellent in heat resistance and light resistance and are relatively inactive.

Antistatic agents applicable to the invention include: Nonionic Antistatic Agents:

Alkylamine derivatives:

e.g. polyoxyethylene alkyl amine, tertiary amines e.g. laurylamine, N,N-bis(2-hydroxyethyl)cocoamine, N-hydroxyhexadecyl-di-ethanolamine, N-hydroxyoctadecyl-di-ethanolamine;

Fatty amide derivatives:

e.g. oxalic acid-N,N'-distearylamine butyl ester, polyoxyethylene alkyl amide;

Ethers:

e.g. polyoxyethylene alkyl ether, polyoxyethylene alkyl phenyl ether;

Polyol esters:

e.g. glycerine fatty acid esters, sorbitan fatty acid esters, 1-hydroxyethyl-2-dodecylglyoxazoline.

Anionic Antistatic Agents:

Sulfonates:

e.g. alkyl sulfonates (RSO_3Na), alkylbenzene sulfonates, alkyl sulfates (ROSO_3Na), etc.

Phosphate esters:

e.g. alkyl phosphates.

Cationic Antistatic Agents:

Cationic amides;

Quaternary ammonium salts:

e.g. quaternary ammonium chlorides, quaternary ammonium sulfates, quaternary ammonium nitrates, e.g. stearamide propyl-dimethyl- β -hydroxyethyl ammonium nitrate.

Ampholytic Antistatic Agents:

Alkyl betaines;

Imidazolines;

Alkyl imidazolines;

Metal salts:

e.g. $(\text{RNR}'\text{CH}_2\text{CH}_2\text{CH}_2\text{NCH}_2\text{COO})_2 \text{Mg}$ ($\text{R} \equiv \text{C}$, $\text{R}' = \text{H}$ or $(\text{CH}_2)_m$ COO^-).

Alkyl alanines;

Conductive resins:

e.g. polyvinylbenzyl cations, polyacrylic acid cations.

Among them, nonionic antistatic agents are particularly preferred, because their adverse effects upon photographic properties are small.

As the antistatic agent for the inside, i.e., when the antistatic agent is blended with a thermoplastic resin, any non-ionic antistatic agent, anionic antistatic agent or ampholytic antistatic agent can be used. Effective nonionic antistatic agents are ethylene oxide adducts of higher alcohols, ethylene oxide adducts of alkyl phenols, esters, such as esters of higher fatty acids and polyols, polyethylene glycol esters of higher fatty acids, polyethers, amides, such as higher fatty amides, dialkyl amides and ethylene oxide adducts of higher fatty amides. Effective anionic antistatic agents are alkyl allylphosphonic acids, adipic acid, glutamic acid, alkyl sulfonic acid salts, alkyl sulfates, polyoxyethylene alkylphosphates, fatty acid salts, alkyl benzene sulfonates, alkyl naphthalene sulfonates, and sodium dialkyl sulfosuccinates. As cationic antistatic agents amines, such as alkyl amine phosphates, Schiff's bases, amide amines, polyethylene imines, complexes of amide amines and metal salts and alkyl esters of amino acids, imidazolines, amine-ethyleneoxide adducts and quaternary ammonium salts are suitable. As ampholytic antistatic agent, for example N-acylsarcosinate, amino carboxylic acid esters, alanine metal salts, imidazoline metal salts, carboxylic acid metal salts, dicarboxylic acid metal salts, diamine metal salts and metal salts having ethylene oxide groups are suitable. Of the other antistatic materials, inorganic electrolytes, metal powders, metal oxides, kaolin, silicates, carbon powder and carbon fiber also exercise the effect of the invention. Besides, graft polymers and polymer blends are also effective.

Among the antistatic agents for the outside, nonionic antistatic agents include polyols, such as glycerine, sorbit, polyethylene glycol and polyethylene oxide; polyol esters, higher alcohol-ethylene oxide adducts, alkylphenol-ethylene oxide adducts, fatty acid-ethylene oxide adducts, amides, amide-ethylene oxide adducts and amine-ethylene oxide adducts; and ampholytic antistatic agents include carboxylic acids, such as alkylalanines, and sulfonic acids. As anionic antistatic agents, carboxylic acid salts, sulfuric acid derivatives, such as alkyl sulfonates, phosphoric acid derivatives, such as phosphonic acid, phosphate esters, and polyester derivatives are suitable. As cationic antistatic agents, e.g. amines, such as alkylamines, amido amines and ester amines, vinyl nitrogen derivatives, quaternary ammonium salts, such as ammonium salts containing amide group and ammonium salts containing ethylene oxide, acrylic acid ester derivatives, acrylic amide derivatives and vinyl ether derivatives, are suitable.

Lubricants applicable to the invention include:

Silicone oil lubricants: silicone oils containing modified siloxane bonds, such as dimethylpolysiloxanes and modifications thereof, polymethylphenyl siloxanes, olefin-modified silicones, polyether-modified silicones modified with polyethylene glycol or polypropylene glycol, olefin/polyether-modified silicones, epoxy-modified silicones, amino-modified silicones and alcohol-modified silicones. Among the above silicone oils, olefin-modified silicones, polyether-modified silicones, and olefin/polyether-modified silicones are excellent.

The silicone oil lubricants provide the basis to obtain a film having good appearance, high sealability and adhesiveness to the article to be packaged without loosening by improving the friction coefficient of the film in heated conditions, resulting in reducing sliding resistance generated during hot plate sealing by an automatic packaging machine and in preventing wrinkling. Besides, reduction of gloss sliding is prevented to obtain a good seal portion. By using a silicone oil lubricant, a high temperature friction coefficient can be decreased to less than 1.4 during sliding heat sealing. A suitable viscosity is 5 to 10 000 cm^2/s (50 to 100,000 centi stokes) at ordinary temperature, and a high viscosity lubricant having a viscosity of 500 to 3000 cm^2/s (5,000 to 30,000 centi stokes) at ordinary temperature is preferred. A suitable content varies according to the object of use, and is in the range of 0.01 to 2.5 wt. %, preferably 0.03 to 1 wt. %, more preferably 0.05 to 0.5 wt. %.

The blending effects of the silicone oil lubricant are:

(1) The silicone oil lubricant coats the surface of fiber fillers, non-fiber light-shielding materials and pigments by blending, and improves their dispersibility.

(2) It improves the fluidity of the resin resulting in the reduction of screw motor load and in the prevention of melt fracture.

(3) A fatty amide lubricant, which is liable to bleed out and induces a white powder problem, can be omitted by blending it.

(4) It decreases the friction coefficient of a film in heated conditions resulting in an improvement of the automatic bag-making ability, in the prevention of wrinkling during heat sealing and of reducing gloss by sliding to obtain a good seal portion.

(5) The light-shielding ability of a light-shielding material is improved by blending together. As a result, the blending amount of the light-shielding material which degrades properties can be reduced.

Examples of saturated fatty amide lubricants are:

Behenic amide lubricants: "DIAMID KN" (tradename, Nippon Kasei Chemical Co., Ltd.);
Stearic amide lubricants: e.g. "ARMIDE HT" (Lion), "ALFLOW S-10" (Nippon Oil and Fats Co., Ltd.), "FATTY AMIDE S" (Kao Corp.), "NEWTRON 2" (Nippon Fine Chemical Co., Ltd.), "DIAMID 200" and "DIAMID AP-1" (Nippon Kasei Chemical Co., Ltd.), "AMIDE S" and "AMIDE T" (Nitto Kagaku K.K.)(all tradenames).

Examples of unsaturated fatty amide lubricants are:

Erucic amide lubricants: e.g. "ALFLOW P-10" (Nippon Oil and Fats Co., Ltd.), "NEWTRON-S" (Nippon Fine Chemical Co., Ltd.), "LUBROL" (I.C.I.), "DIAMID L-200" (Nippon Kasei Chemical Co., Ltd.)(all tradenames);
Oleic amide lubricants: e.g. "ARMOSLIP-CP" (Lion Akzo Co., Ltd.), "NEWTRON" and "NEWTRON E-18" (Nippon Fine Chemical Co., Ltd.), "AMIDE-O" (Nitto Kagaku K.K.), "DIAMID O-200" and "DIAMID G-200" (Nippon Kasei Chemical Co., Ltd.), "ALFLOW E-10" (Nippon Oil and Fats Co., Ltd.), "FATTY AMIDE O" (Kao Corp.)(all tradenames).

Examples of bis fatty amide lubricants are:

Methylene bis behenic amide lubricants: e.g. "DIAMID NK BIS" (tradename, Nippon Kasei Chemical Co., Ltd.);
Methylene bis stearic amide lubricants: e.g. "DIAMID 200 BIS" (Nippon Kasei Chemical Co., Ltd.), "ARMOWAX" (Lion Akzo Co., Ltd.), "BISAMIDE" (Nitto Kagaku K.K.) (all tradenames);
Methylene bis oleic amide lubricants: "LUBRON O" (tradename, Nippon Kasei Chemical Co., Ltd.);
Ethylene bis stearic amide lubricants: "ARMOSLIP EBS" (tradename, Lion Akzo Co., Ltd.);
Hexamethylene bis stearic amide lubricants: "AMIDE 65" (tradename, Kawaken Fine Chemicals Co., Ltd.);
Hexamethylene bis oleic amide lubricants: "AMIDE 60" (tradename, Kawaken Fine Chemicals Co., Ltd.).

Examples of monoalkylol amide lubricants are:

N-(2-Hydroxyethyl)lauric amide lubricants: e.g. "TOHOL N 130" (tradename, Toho Chemical Ind. Co., Ltd.);
N-(2-Hydroxyethyl)stearic amide lubricants: "AMISOL" (tradename, Kawaken Fine Chemicals Co., Ltd.);
N-(2-Hydroxymethyl)stearic amide lubricants: "METHYLOL AMIDE" (tradename, Nitto Kagaku K.K.).
Examples of nonionic surfactant lubricants are: "ELECTROSTRIPPER TS-2", "ELECTROSTRIPPER TS-3" (Kao Corp.)(tradenames).
Examples of hydrocarbon lubricants are: liquid paraffin, natural paraffin, microwax, synthetic paraffin, polyethylene wax, polypropylene wax, chlorinated hydrocarbons and fluorocarbons.
Examples of fatty acid lubricants are: higher fatty acids preferably more than C₁₂ and hydroxy fatty acids.
Examples of ester lubricants are: fatty acid lower alcohol esters, fatty acid polyol esters, fatty acid polyglycol esters and fatty acid fatty alcohol esters.
Examples of alcohol lubricants are: polyols, polyglycols and polyglycerols.
Examples of metallic soaps are: metal salts, such as Li, Mg, Ca, Sr, Ba, Zn, Cd, Al, Sn, Pb salts, of higher fatty acids, such as lauric acid, stearic acid, ricinoleic acid, naphthenic acid, oleic acid.

A suitable content of the lubricant is 0.01 to 5 wt. %, and in the case of fatty amide lubricants having a great lubricating ability and being liable to bleed out, a suitable content is 0.01 to 1 wt. %, and preferably decreases to a minimum content.

The laminated film of the invention may be laminated with a flexible sheet through or without an adhesive layer. A suitable flexible sheet has a Young's modulus (ASTM D-882) of more than 50 kg/mm² and has heat resistance (which means a flexible sheet having a melting point of more than 100°C or no melting point, such as paper, cellophane and cloth).

Suitable flexible sheets are various thermoplastic resin films such as various polyethylene resin films, ethylene copolymer resin films, polypropylene resin films, polyvinyl chloride resin films, polyvinylidene chloride resin films, poly-

5 midel resin films, polycarbonate resin films, polyester resin films their modified resin films, and uniaxially or biaxially stretched films thereof. Cellulose acetate films, cellophane regenerated cellulose films, ethylene-vinyl alcohol copolymer resin films (Eval resin films), paper, synthetic paper and nonwoven fabrics, are also suitable. Preferable flexible sheets are various papers having heat resistance, no melting point, no adverse affect upon photosensitive materials, and an areal weight of 20 to 400 g/m², such as unbleached kraft paper, semibleached kraft paper, bleached kraft paper, high yield pulp paper, neutral paper, twisting paper, Clupak paper, Duostress paper, white cardboard, photo base paper, pure white roll paper, coated paper, waste paper, regenerated paper, simili and glassine paper.

10 The above papers may be provided with various printings, various surface treatments, such as coatings of a pigment layer, coatings of a resin layer and metallization, and colorings. Various light-shielding materials may be blended in order to impart light-shielding ability, or may be provided with various embossings.

Other preferable heat-resistant flexible sheets are biaxially stretched thermoplastic resin films and cellophane. Uniaxially stretched thermoplastic resin films are also preferred according to the use of the laminated film.

15 The biaxially stretched thermoplastic resin film is produced by a known biaxial drawing method such as simultaneously biaxial drawing or successively biaxial stretching, and both of the drawing ratios in longitudinal direction (MD) and in lateral direction (CD) are 1.5 to 20 times, preferably 3 to 15 times, respectively. The resin suitable for the film includes polyester resins, polyamide (nylon) resins, polyethylene resins, polystyrene resins, polypropylene resins, polyolefin copolymer resins, polyvinyl chloride resins, polyvinylidene chloride resins, ethylene-vinyl alcohol copolymer resins, ethylene-vinyl acetate copolymer saponified resins, polyacrylonitrile resins, vinylon resins, copolymer resins of the above resins and other resins, including binary, ternary or more copolymers polymerized by random copolymerization or block copolymerization, and resin blends of the above resins and other resins. The resin used for the uniaxially stretched thermoplastic resin film may be selected from the above resins. The above polyester resin includes the resins e.g. synthesized from dimethyl terephthalate and ethylene glycol, dimethyl terephthalate and 1,4-cyclohexanedimethanol, or dimethyl terephthalate and dimethyl isophthalate. The polyamide resin includes e.g. nylon 6, nylon 66, nylon 11 and nylon 6-66 copolymers. The biaxially stretched film is produced by a T die film molding machine or an inflation film molding machine wherein the resin is molded into a film and then drawn biaxially.

25 The uniaxially or biaxially stretched thermoplastic resin film and cellophane may be provided with metallizing, coatings of a polyvinylidene chloride resin layer, various printings or various colorings. They may also be provided with various embossings in order to improve the slipping characteristics or the printability.

30 A suitable thickness of the biaxially stretched thermoplastic resin film is 5 to 70 μm , preferably 7 to 50 μm , more preferably 10 to 35 μm in order to make the packaging material thin, to decrease the costs and to ensure flexibility and physical strength. When the thickness is less than 5 μm , wrinkling and breakage of the film tend to occur in the laminating process. When the thickness exceeds 70 μm , the film is stiff resulting in the degradation of the bag-making ability. Gelbo test strength and handling are also degraded. The Young's modulus of the flexible sheet is preferably higher than 50 kg/mm², more preferably higher than 80 kg/mm², and a Young's modulus of more than 100 kg/mm² is particularly preferred. The heat resistance of the flexible sheet is preferably higher than that of the outer layer by 50°C or more, preferably 100°C or more, in view of the improvement in bag-making ability and appearance. Examples of suitable flexible sheets are:

	Young's Modulus (kg/mm ²)	Melting Point (°C)
Biaxially Stretched HDPE film	80-90	137
Unstretched polypropylene film	60-90	140
Biaxially stretched polypropylene film	150-350	175
Polyvinylidene chloride-coated		
Biaxially stretched polypropylene film	170-260	175
Biaxially stretched polyamide film	130-280	225
Biaxially stretched polyester film	190-400	260
Cellophane	140-210	150 (Carbonized)
Polyvinylidene chloride-coated cellophane	160-320	150 (Carbonized)
Ethylene-vinyl alcohol copolymer film	190-350	180
Biaxially stretched polystyrene film	280-390	160
Polycarbonate film	280-240	220
Cellulose acetate film	50-280	>260
Kraft paper	>350	>260

The flexible sheet is laminated to the outer layer through or without an adhesive layer. The adhesive layer may for example be formed by the wet laminating, the dry laminating, the hot melt laminating, the extrusion laminating or the coextrusion laminating method. Preferred adhesive layers are extrusion laminated adhesive layers containing more than 50 wt. % of at least one of thermoplastic resin of which the content of volatile components which adversely affect photographic photosensitive materials is small, particularly polyolefin resins, such as low density homopolyethylene resins, L-LDPE resins, EEA resins, EAA resins, EVA resins, acid-modified polyolefin resins and propylene copolymer resins. A suitable thickness of the adhesive layer is 1 to 50 μm , preferably 2 to 30 μm , particularly preferably 3 to 10 μm . When the thickness is less than 1 μm , the adhesive force cannot be ensured due to the occurrence of membrane rupture. When the thickness exceeds 50 μm , neck-in occurs greatly.

The laminated film of the invention may be laminated with a heat sealing layer. The heat sealing layer has a Vicat softening point (ASTM D-1525) lower than the outer layer by 5°C or more, preferably 10°C or more. A heat sealing layer having a Vicat softening point lower than the outer layer may be laminated directly or through an adhesive layer. Suitable resins for the heat sealing layer are various thermoplastic resins having heatsealability, and various polyolefin resins. Particularly low density homopolyethylene resin and various ethylene copolymer resins are preferred. Preferable ethylene copolymer resins are the same as disclosed regarding the inner layer. Particularly preferred resins are also the L-LDPE resins and EEA resins disclosed regarding the inner layer; and L-LDPE resins are most preferable. In order to adjust the properties to be necessary, it is preferred to blend said resins with other thermoplastic resins, elastomers, rubbers, various additives or modifiers. By incorporating more than 5 wt. %, preferably more than 10 wt. % of an ethylene copolymer resin, the decrease of the heat sealing strength with time can be prevented.

The laminated film of the invention is usable as a packaging material, such as various packaging bags for various photosensitive materials, foods, medicines, dyes, resins, agricultural products, fish meals, fertilizers, cements, and explosives; covering films for commercial goods; multilayers for agricultural chemicals, water-proof films; moistureproof films; light-shielding films; low temperature-resistant films and heat-resistant films.

The laminated film of the invention is suitable for packaging the following photosensitive materials.

Silver halide photographic photosensitive materials:

e.g. photographs for roentgenograms, films for printing (lithfilms), monochromatic and color photographic printing papers, color films, master papers for printing, DTR photosensitive materials, films and papers for computerized type-setting systems, microfilms, films for movies, self-developing type photographic photosensitive materials, direct positive films and papers;

Diazonium photographic photosensitive materials:

e.g. 4-morpholinobenzene diazonium microfilms, microfilms, copying films, form plates for printing;

5 Azide, diazide photographic photosensitive materials:

e.g. photosensitive materials containing parazidobenzoate or 4,4'-diazidostilbene, such as copying films and form plates for printing;

10 Quinone diazide photographic photosensitive materials:

e.g. photosensitive materials containing ortho-quinone diazide compounds or ortho-naphthoquinone diazide compounds, such as benzoquinone-(1,2)-diazido-(2)-4-sulfonic acid phenyl ether, such as form plates for printing, copying films and contact printing films;

15 Photo polymers: e.g. photosensitive materials, form plates for printing, contact printing films containing vinyl compound monomers;

Polyvinyl cinnamate esters: e.g. printing films, photoresists for IC.

20 Moreover, the packaging material of the invention is also applicable to various photosensitive materials which can e.g. be degraded or denatured by light, oxygen or sulfur dioxide gas, such as foods including peanuts with butter, margarine, snacks, relishes, cakes, teas and lavers, medicines including powder and granular medicines placed in a bag for stomach and bowels and for cold, ABS resin, dyes, pigments, photographic developing agent, photographic fixing agent and toners.

25 The package form for example includes a single-sheet flat bag, a double-sheet flat bag, a self-standing bag, a single-sheet gusset bag, a double-sheet gusset bag, a standing pouch, a satchel bag, a laminated film, an inner lining for a moistureproof box, an inner lining for a light room-loading light-shielding box, a light-shielding member for magazine-less light room-loading, and a leader paper. The bag-making may be conducted according known adhesion methods of plastic films, such as hot plate welding, impulse welding, ultrasonic welding and high frequency welding. The methods of using an adhesive and the methods of using a pressure-sensitive adhesive or a heat-sensitive adhesive may also be used.

30 Taking into consideration the disposal of the materials, to blend a degradable plastic is preferred, such as biodegradable polymers (e.g. "BIOPOL" (tradename), ICI, polycaprolactone, UCC.). To blend natural or synthetic polymers which are biodegradable, such as starch, various ethylene copolymer resins, and various polyethylene resins is also applicable. Photodegradable polymers are also applicable, such as a ECO copolymer which is a polyethylene the main chain of which contains carbonyl groups as the photosensitive groups, produced by copolymerization of ethylene and CO gas, and various photodegradable polymers the photodegradation ability of which is imparted by blending a e.g. transition metal salt, an oxidation accelerator or a photosensitizer.

Some embodiments of the laminated film of the invention are shown in Figures 1 through 27.

40 The laminated film 8a of Figure 1 is formed of a single layer inflation film composed of a light-shielding inner layer 1a which is deflated and joined by blocking B. The laminated film 8 is cut into two webs, and the joined inner layer portion at the cut end forms a heat fused portion 2 to ensure joining. The inner layer may not contain a light-shielding material.

45 The laminated film 8a of Figure 2 is formed of a coextruded double layer inflation film 9a composed of a light-shielding inner layer 1a and a light-shielding outer layer 3a which is deflated and joined by blocking B. The laminated film 8 is cut into two webs, and the joined inner layer portion at the cut end forms a heat fused portion 2 to ensure joining. The inner layer and outer layer may not contain a light-shielding material.

50 The laminated film 8a of Figure 3 is formed of a coextruded triple layer inflation film 10a composed of a light-shielding inner layer 1a, a light-shielding outer layer 3a and a middle layer 4 which is deflated and joined by blocking B. The laminated film 8 is cut into two webs, and the joined inner layer portion at the cut end forms a heat fused portion 2 to ensure joining. Every layer may or may not contain a light-shielding material.

The laminated film of Figure 4 is the same as that of Figure 1 of which the other end is also cut off, and forms a heat fused portion 2.

55 The laminated film of Figure 5 is the same as that of Figure 2 of which the other end is also cut off, and forms a heat fused portion 2.

The laminated film of Figure 6 is the same as that of Figure 3 of which the other end is also cut off, and forms a heat fused portion 2.

The laminated film of Figure 7 is composed of the laminated film of Figure 2 and a flexible sheet 6 laminated thereon through an adhesive layer 5.

The laminated film of Figure 8 is composed of the laminated film of Figure 3 and a heat sealing layer 7 directly laminated thereon by extrusion laminating.

In the laminated films 11a of Figures 9 through 15, the inner layer contains a thermoplastic resin having a Shore hardness lower than the resin of the outer layer and/or the inner layer contains an acid-modified polyolefin resin.

The laminated film of Figure 9 is formed of a coextruded double layer inflation film 9a composed of a light-shielding inner layer 1a and an outer layer 3 which is deflated and joined by blocking B.

The laminated film of Figure 10 is the same as that of Figure 9, except that the outer layer 3a also contains a light-shielding material.

The laminated film of Figure 11 is composed of the laminated film of Figure 9 and a heat sealing layer 7 directly laminated thereto.

The laminated film of Figure 12 is composed of the laminated film of Figure 9 and a metallized flexible sheet layer 14 of a heat-resistant flexible sheet 12 (13 is a metal membrane layer) laminated through an adhesive layer 5.

The laminated film of Figure 13 is formed of a coextruded triple layer inflation film 10a composed of a light-shielding inner layer 1a, a middle layer 4 and an outer layer 3 which is deflated and joined by blocking B.

The laminated film of Figure 14 is composed of the laminated film of Figure 13 and a heat sealing layer 7 laminated thereonto through an adhesive layer 5a containing a light-shielding material.

The laminated film of Figure 15 is composed of the laminated film of Figure 13 and a heat-resistant flexible sheet layer 12 laminated thereonto through an adhesive layer 5.

Figure 16 illustrates a whole section of a laminated film formed of a coextruded double layer inflation film 9a composed of a light-shielding inner layer 1a and a light-shielding outer layer 3a which is deflated and joined by blocking B. The positions indicated by an arrow are slitted by a heated razor to obtain the laminated film of Figures 2 and 5.

Figures 17 through 21 illustrate various patterns of the strongly joined portions.

In the laminated film 15 of Figure 17, the strongly joined portions S are formed into spots in the weakly joined portion W.

In the laminated film 15 of Figure 18, the strongly joined portions S are formed into streaks in the longitudinal direction in the weakly joined portion W.

In the laminated film 15 of Figure 19, the strongly joined portions S are formed into streaks in the lateral direction in the weakly joined portion W.

In the laminated film of Figure 20, the strongly joined portions S are formed into lattice in the weakly joined portion W.

In the laminated film of Figure 21, the strongly joined portion S are formed into streaks in an oblique direction.

Figures 22 through 28 illustrate various laminated films 16a wherein the end portions are joined more strongly than the central portion.

The laminated film 16a of Figure 22 is produced by superposing two single layer sheets composed of a light-shielding inner layer 1a, blocking the faced portion to form the weakly joined portion W, and pressing both end portions to form the strongly joined portions S by blocking.

The laminated film of Figure 23 is produced by turning up a single layer sheet composed of a light-shielding inner layer 1a, blocking the faced portion to form the weakly joined portion W, and pressing the end portion opposite to the folded end to form the strongly joined portion S by blocking.

The laminated film of Figure 24 is composed of the laminated film of Figure 22 and a flexible sheet laminated thereon through an adhesive layer 5.

The laminated film of Figure 25 is the same as that of Figure 22 except that both superposed sheets are not a single layer sheet but a coextruded double layer film 9a composed of a light-shielding inner layer 1a and a light-shielding outer layer 3a.

The laminated film of Figure 26 is composed of the laminated film of Figure 25, wherein both of the inner layer 1 and the outer layer 3 do not contain a light-shielding material, and a heat sealing layer 7a containing a light-shielding material directly laminated thereonto.

The laminated film of Figure 27 is composed of the laminated film of Figure 25, wherein the inner layer 1 does not contain a light-shielding material, and a metallized flexible sheet layer 14 laminated thereon through an adhesive layer 5.

The laminated film of Figure 28 is the same as that of Figure 22 except that both superposed sheets are not a single layer sheet but a coextruded triple layer film 10a composed of a light-shielding inner layer 1a, a middle layer 4 and an outer layer 3.

The laminated film formed of an inflation film of which the inner surface is joined by blocking can be produced, for example, by the inflation film molding apparatus 20 shown in Figure 29. In the apparatus, molten resins are co-extruded from a ring die 21, and inflated by air. The inflated tubular film 22 travels upward, and is deflated by passing a nip roll 23. At that time, the inner layer 1a of the coextruded double layer inflation film 9a is joined by blocking B as shown in circle Y.

The laminated film wherein the cut end is joined by heat fusion can be produced, for example, by the cutting appa-

ratus 30 shown in Figure 30. This apparatus 30 is provided on the down stream side of the inflation film molding apparatus 20. The inflation tubular film 22 is deflated and the inner layer is joined by blocking during passing the nip roll 23. The laminated film joined by blocking travels horizontally, and then turns downward. Two heated razor blades 31,31 are provided so as to slit the traveling laminated film into an equal width. The heated razor blades 31 are heated by an electric heater so that the blades are adjusted to a prescribed temperature in the range of 50°C to the melting point of the film 8a, preferably around the softening point of the film. A temperature higher than the softening point of the inner layer is particularly preferred. 33 is an ion sputter for eliminating static electricity generated at the contact portion of each blade with the film caused by the friction. The laminated film is slitted into three webs 8a by the blades 31, and then taken up into rolls 34. A section of the slitted film is shown in Figure 31. As shown in the figure, the outer end of the blocking portion forms a heat fused portion 2, and the outer edge 35 is slightly thickened.

The laminated film 15 having a pattern of the strongly joined portions shown in Figure 19 can be produced by using the apparatus shown in Figure 32, heating the laminated film joined by blocking by a heater 41 and then passing a pair pressure rolls composed of an embossing roll 42 of which the surface is formed with ribs 43 in the axial direction at regular intervals and a flat roll 44.

The laminated film 15 having a pattern of the strongly joined portions shown in Figure 20 can be produced by using the apparatus shown in Figure 33, heating, passing a first embossing roll 45 having ribs 46 in the circumferential direction to form the strongly joined streaks S in the longitudinal direction, and then passing the second embossing roll 47 having ribs 48 in the axial direction to form the strongly joined streaks S in the lateral direction.

The laminated film 16 wherein the end portions are joined more strongly than the central portion can be produced by the apparatus 50 shown in Figure 34. This apparatus is the same as the cutting apparatus 30 of Figure 30 wherein two embossing rolls 51,51 having an obliquely lattice projection pattern on the surface are provided so as to partition the laminated film by blocking into three parts in the longitudinal direction. The embossing rolls 51 are heated by a heater 52 to higher than the Vicat softening point of the inner layer of the laminated film. A support roll 53 which is a heat-resistant elastic roll is provided under the embossing rolls 51 so as to nip the traveling laminated film by the support roll 53 and the embossing rolls 51. Two strongly joined lines 54 are formed by passing the laminated film through the heated embossing rolls 51. Then, the laminated film is slitted into three webs 16a having a section of Figure 22 or 23, and then taken up into rolls 55.

The cutting apparatus of Figure 30 can be used for edge trimming by changing the position of the heated razor blades 31, as shown in Figure 35. The deflated inflation film is not laminated by blocking as usual, and edge-trimmed films 61 are wound separately. The cut end 62 is slightly thickened as shown in Figure 36.

Another cutting apparatus 70 capable of forming a heat fused portion at cut ends is shown in Figure 37. In this apparatus, the cutting portion is composed of fixed heated razor blades 71 heated by a heater 72 and a fixed roll 73 with channels 74.

In the above cutting apparatuses, the means to eliminate static electricity is not limited to the iron sputter but includes using a corona discharge apparatus, contacting the surface of the laminated film with a metal lace, a conductive film or a conductive knitted, woven or nonwoven fabric composed of conductive fibers, such as metal fibers or carbon fibers.

EXAMPLES

Example 1

A laminated film, the inner surface of which is joined by blocking and the cut end is joined by heat fusion was prepared from a coextruded double layer inflation film.

The outer layer was composed of an ethylene-hexene-1 copolymer resin having a MI (ASTM D-1238, at 190°C) of 2.1 g/10 minutes, a density (ASTM D-1505, at 23°C) of 0.920 g/cm³, a Vicat softening point (ASTM D-1525) of 102°C and a Shore hardness (ASTM D-2240) of 55 D, containing 15 wt. % of a homopolyethylene resin having a MI of 1.2 g/10 minutes, a density of 0.950 g/cm³, a Vicat softening point of 123°C and a Shore hardness of 69 D, 2 wt. % of oil furnace carbon black having a mean particle size of 21nm (m μ), 0.2 wt. % of a monoglycerine ester, 0.05 wt. % of dimethylpolysiloxane having a viscosity of 1000 cm²/s (10,000 centi stokes) and 0.1 wt. % of 5,8-dimethyl-tocotrienol, and had a thickness of 20 μ m.

The inner layer was composed of an ethylene-butene-1 copolymer resin having a MI of 1.0 g/10 minutes, a density of 0.89 g/cm³, a Shore hardness of 38 D and a Vicat softening point of 75°C, containing 5 wt. % of a cumarone-indene resin, 3 wt. % of oil furnace carbon black having a mean particle size of 21nm (m μ), 0.05 wt. % of dimethylpolysiloxane having a viscosity of 1000 cm²/s (10,000 centi stokes) and 0.05 wt. % of 5,8-dimethyl-tocotrienol, and had a thickness of 30 μ m.

The above inflation film was molded into a cylindrical tubular film by coextruding from the ring die of an inflation film molding machine at a blow-up ratio of 1.4, and the outer layer was heated by a far-infrared lamp at the position immediately under the guide plate so that the surface temperature became 40 to 70°C. The inner layer of the tubular film was

joined by blocking during passing the squeeze roll (nip roll), as shown in Figure 16, and then slitted into three webs each having a width of 50 cm by a heated razor blade which was heated to 80°C by its electric resistance to obtain the laminated films shown in Figures 1 and 4.

The laminated film was not separated from the cut end over the bag making process, and had a suitable adhesive strength of 20 g/15 mm width, a tear strength of more than 1,600 g in both of the longitudinal and lateral directions, and a Gelbo test strength of more than 300 times. Curling was very small. The laminated film was suitable for light-shielding bags for articles, and put to practical use as a light-shielding bag for a roll of movie film having sharp edges [35 mm x 914.4m (3,000 ft)]. Compared with the conventional laminated film produced by laminating two light-shielding LDPE films of 70 μ m in thickness onto both sides of a cross-laminated porous fabric through a longitudinal streak adhesive layer, the costs of the laminated film was reduced to less than a half. Since the laminated film had a suitable rigidity, no curling and contained dimethylpolysiloxane in the outer layer, the friction coefficient of the film in the heated conditions was small. The laminated film was excellent in bag-making ability by an automatic bag-making machine, heat sealing properties, such as sealability with other materials, hot tack properties, heat sealing strength and heat sealing strength with time, and insertion of the article to be packaged.

Moreover, it was found that the light-shielding ability and antioxidation ability were sharply improved by combining dimethylpolysiloxane, carbon black and 5,8-dimethyl-tocotrienol by their synergistic effect. Dimethylpolysiloxane [Viscosity: 1000 cm²/s (10,000 centi stokes)] used as a lubricant improved the dispersibility of carbon black without adversely affecting the photographic properties, improved the slipping characteristics, decreased the friction coefficient of the laminated film in the heated conditions without the generation of white powder due to bleeding out of the lubricant, which occurs if fatty amide are used, and the occurrence of wrinkling and the reduction of gloss could be prevented.

Example 2

A laminated film, the inner surface of which is joined by blocking and the cut end is joined by heat fusion was prepared from a single layer inflation film 50 μ m in thickness.

The resin composition was composed of 87.65 wt. % of an ethylene-4-methylpentene-1 copolymer resin having a MI of 2.1 g/10 minutes, a density of 0.920 g/cm³, a Vicat softening point of 100°C and a Shore hardness of 56 D, 10 wt. % of a homopolyethylene resin having a MI of 1.1 g/10 minutes, a density of 0.954 g/cm³, a Vicat softening point of 126 °C and a Shore hardness of 69 D, 2 wt. % of oil furnace carbon black having a mean particle size of 21 nm (m μ), 0.2 wt. % of a nonionic antioxidant ("Electrostripper TS-2", tradename), 0.05 wt. % of dimethylpolysiloxane having a viscosity of 1000 cm²/s (10,000 centi stokes) and 0.1 wt. % of 5,8-dimethyl-tocotrienol.

The above inflation film was molded by using an inflation film molding machine at a blow-up ratio of 1.2 into a cylindrical tubular film. After passing the guide plate, the tubular film was pressed by passing a pressure mat roll with 0.3mm (50 mesh)(squeeze roll for taking up) heated to 100°C to obtain a laminated film 97 μ m in thickness wherein the inner layer was partially strongly joined.

The laminated film was not separated from the cut end during the bag making process. The tear strength was more than 1,600 g, and the Gelbo test strength was more than 300 times. The laminated film was excellent in heat sealing properties, bag-making ability and insertion of the article to be packaged, similar to Example 1.

Comparative Example 1

A laminated film was prepared using the resin composition of Example 2 wherein 0.05 wt. % of dimethylpolysiloxane having a viscosity of 1000 cm²/s (10,000 centi stokes) and 0.1 wt. % of 5,8-dimethyl-tocotrienol were not added by the same method as Example 2, except that the tubular film passed a common squeeze roll for taking out having a flat surface instead of the heated pressure mat roll, and slitted by a razor at ordinary temperature. In the inflation film, the inner layer was not joined. The light-shielding ability of the inflation film was insufficient, and fogging by light occurred.

Example 3

The layer construction corresponds to Figure 9.

The inner layer was composed of 75.8 wt. % of an ethylene-octene-1 copolymer resin having a MI of 2.5 g/10 minutes, a density of 0.92 g/cm³, a Vicat softening point of 98°C and a Shore hardness of 58 D, 20 wt. % ethylene-vinyl acetate type acid-modified polyolefin resin having a MI of 2.4 g/10 minutes, a density of 0.94 g/cm³, a Vicat softening point of 59°C and a Shore hardness of 35 D, 3 wt. % of oil furnace carbon black of pH 7.7 having a mean particle size of 21 nm (m μ), 1.0 wt. % of calcium stearate, 0.1 wt. % of a phenol antioxidant and 0.1 wt. % of a phosphorus-containing antioxidant, and had a thickness of 25 μ m, a Shore hardness of 52 D and a Vicat softening point of 92°C.

The outer layer was composed of 71.7 wt. % of an ethylene-4-methylpentene-1 copolymer resin having a MI of 2.1 g/10 minutes, a density of 0.92 g/cm³, a Shore hardness of 57 D and a Vicat softening point of 100°C, 10 wt. % of a

homopolyethylene resin, 15 wt. % of an ethylene-4-methylpentene-1 copolymer resin having a MI of 2.1 g/10 minutes, a density of 0.94 g/cm³, a Shore hardness of 63 D and a Vicat softening point of 118°C, 3 wt. % of oil furnace carbon black of pH 7.7 having a mean particle size of 21nm (m_μ), 0.3 wt. % of an antistatic agent ("Electrostripper TS-2", trade-name), and had a thickness of 25 μm, a Shore hardness of 62 D and a Vicat softening point of 116°C.

The above inflation film of 50 μm in total thickness was molded by an inflation film molding machine into a cylindrical tubular film, and the surface of the outer layer was air-cooled. Then, it was heated again to 60°C by a ring form far-infrared lamp at the position on the down stream side by 1.5 m from the frost line. The inflation film was passed through the usual nip roll of the inflation film molding machine, and the inner layer of the inflation film was joined by blocking to obtain a symmetrical laminated film of 100 μm thickness composed of four layers.

Example 4

The layer construction corresponds to Figure 10.

The resin composition of the inner layer was the same as the inner layer of Example 3, and the thickness was 40 μm.

The outer layer was composed of 20 wt. % of a L-LDPE type acid-modified polyolefin resin having a MI of 1.3 g/10 minutes, a density of 0.94 g/cm³, a Shore hardness of 56 D, a Vicat softening point of 100°C and a melting point of 120 °C, and 80 wt. % of a nylon 66 resin ("Leona", tradename), and had a thickness of 10 μm, a Rockwell hardness (ASTM D-785) of 119 R and a Vicat softening point of 198°C.

The surface of the outer layer of the above coextruded double layer inflation film of 50 μm in thickness was air-cooled, and the inner layer was contacted with a water-cooled mandrel (cooling water temperature: 10°C). After the bubble became stable, the inner layer of the inflation film was joined by blocking by passing the usual nip roll of the inflation film molding machine to obtain a symmetrical laminated film composed of four layers.

Example 5

The layer construction corresponds to Figure 9.

This laminated film was the same as the laminated film of Example 3, except that the ethylene-vinyl acetate type acid-modified polyolefin resin was replaced by a L-LDPE type acid-modified polyolefin resin having a MI of 6.2 g/10 minutes, a density of 0.91 g/cm³, a Shore hardness of 46 D, a Vicat softening point of 91°C and a melting point of 112 °C. As a result, the Shore hardness of the inner layer was changed to 55 D, and the Vicat softening point was changed to 96°C.

Example 6

The layer construction corresponds to Figure 9.

This laminated film was the same as the laminated film of Example 3, except that the ethylene-vinyl acetate type acid-modified polyolefin resin was replaced by a LDPE type acid-modified polyolefin resin having a MI of 1.1 g/10 minutes, a density of 0.90 g/cm³, a Shore hardness of 50 D, a Vicat softening point of 92°C and a melting point of 110 °C. As a result, the Shore hardness of the inner layer was changed to 56 D, and the Vicat softening point was changed to 97°C.

Example 7

The layer construction corresponds to Figure 12.

This laminated film had a six layer construction composed of the same laminated film joined by blocking of Example 3, and an aluminum-metallized biaxially stretched polyester resin film of 10 μm in thickness having a Young's modulus of 218 kg/mm², a melting point of 260°C and an aluminum membrane 40nm (400 Å) thick laminated thereon through a polyolefin adhesive layer of 15 μm in thickness composed of 15 wt. % of a L-LDPE type acid-modified polyolefin resin having a MI of 9 g/10 minutes, a density of 0.93 g/cm³, a Shore hardness of 53 D, a Vicat softening point of 95°C and a melting point of 120°C and 85 wt. % of a high pressure branched homopolyethylene resin having a MI of 7 g/10 minutes, a density of 0.92 g/cm³, a Shore hardness of 51 D and a Vicat softening point of 92°C provided by extrusion laminating at the resin temperature of 300°C, so that the aluminum membrane layer faced the outer layer.

Example 8

The layer construction is similar to Figure 12.

This laminated film was the same as that of Example 7, except that the aluminum-metallized biaxially stretched polyester resin film was replaced by a biaxially stretched film having a Young's modulus of 210 kg/mm² and a melting point

of 120°C, called KOP film, which was composed of a biaxially stretched polypropylene resin film of 20 µm in thickness, both faces of which were coated with a polyvinylidene chloride resin layer of 1.5 µm in thickness.

Example 9

The layer construction corresponds to Figure 12.

This laminated film was the same as that of Example 7, except that the aluminum-metallized biaxially stretched polyester resin film was replaced by an aluminum-metallized biaxially stretched nylon film of 15 µm in thickness having a Young's modulus of 246 kg/mm² and a melting point of 220°C.

Example 10

The layer construction corresponds to Figure 11.

This laminated film had a five layer construction composed of the same laminated film joined by blocking of Example 4, and a light-shielding heat sealing layer of 30 µm in thickness composed of 10 wt. % of a L-LDPE type acid-modified polyolefin resin having a MI of 3.5 g/10 minutes, a density of 0.93 g/cm³, a Shore hardness of 53 D, a Vicat softening point of 98°C and a melting point of 120°C, 57 wt. % of a high pressure branched homopolyethylene type acid-modified polyolefin resin having a MI of 7 g/10 minutes, a density of 0.92 g/cm³, a Shore hardness of 51 D and a Vicat softening point of 92°C, 30 wt. % of an ethylene-butene-1 copolymer resin having a MI of 15 g/10 minutes, a density of 0.92 g/cm³, a Shore hardness of 56 D and a Vicat softening point of 105°C and 3 wt. % of oil furnace carbon black of pH 7.7 having a mean particle size of 21nm (mµ) provided by extrusion laminating at the resin temperature of 320°C.

Comparative Example 2

The layer construction is similar to Figure 9.

This laminated film was the same as the reversed laminated film of Example 3, i.e. the inner layer of Example 3 was used as the outer layer and the outer layer of Example 3 was used as the inner layer.

Comparative Example 3

The layer construction is similar to Figure 9.

This laminated film had a thickness of 100 µm, and was composed of an outer layer which was the same as the outer layer of Example 3, and an inner layer of 25 µm in thickness which was composed of 96.9 wt. % of a commercial ethylene-octene-1 copolymer resin ("Stamilex", DSM) having a MI of 2.0 g/10 minutes, a density of 0.92 g/cm³, a Shore hardness of 57 D and a Vicat softening point of 108°C, 0.1 wt. % of oleic amide and 3 wt. % of oil furnace carbon black of pH 7.7 having a mean particle size of 21 nm (mµ). The inner layers were joined by blocking.

Properties of the laminated films of Examples 3 to 10 and Comparative Examples 2 and 3 are summarized in Table 1.

Table 1

Unit Example3 Example4 Example5 Example6 Example7 Example8 Example9 Example10 Comparative2 Comparative3 Test Method													
Layer Construction	-	Fig.9	Fig.10	Fig.9	Fig.9	Fig.12	Similar to Fig.12	Fig.12	Fig.11	Similar to Fig.9	Similar to Fig.9	Similar to Fig.9	-
Inner Layer Thickness	μm	25	40	25	25	25	25	25	40	25	25	25	JIS P-8118
Shore Hardness	D	52	52	55	56	52	52	52	52	63	63	57	ASTM D-2240
Vicat Softening point	$^{\circ}\text{C}$	92	92	96	97	92	92	92	92	116	116	108	ASTM D-1525
Outer Layer Thickness	μm	25	10	25	25	25	25	25	10	25	25	25	JIS P-8118
Shore or Rockwell Hardness	D	63	-	63	63	63	63	63	-	52	52	63	ASTM D-785
Vicat Softening point	$^{\circ}\text{C}$	116	198	116	116	116	116	116	198	92	92	116	ASTM D-1525
Inflation Film Number of Layers	-	2	2	2	2	2	2	2	2	2	2	2	-
Thickness	μm	50	50	50	50	50	50	50	50	50	50	50	JIS P-8118
Thickness of Laminated Film by Blocking	μm	100	100	100	100	100	100	100	100	100	100	100	JIS P-8118
Adhesive Layer Thickness	μm	-	-	-	-	-	15	15	-	-	-	-	JIS P-8118
Laminated Flexible Sheet													
Kind	-	-	-	-	-	-	Al metallized biaxially stretched polyester resin film	KOP film	Al metallized biaxially stretched nylon resin film	-	-	-	-
Thickness	μm	-	-	-	-	-	10	20	15	-	-	-	JIS P-8118
Young's Modulus	kg/mm^2	-	-	-	-	-	218	210	246	-	-	-	ASTM D-882
Melting Point	$^{\circ}\text{C}$	-	-	-	-	-	260	120	220	-	-	-	DSC Method
Heat Sealing Layer Thickness	μm	-	-	-	-	-	-	-	-	30	-	-	JIS P-8118
Separation at Out End Portion	-	None	None	None	None	None	None	None	None	No automatic bag-making	No automatic bag-making	No automatic bag-making	*1
Wrinkling, Streaks, Blister	-	None	None	None	None	None	None	None	None	Occur	Occur	Occur	
Resistance to Punctures	-	Very Excellent	Very Excellent	Very Excellent	Very Excellent	Very Excellent	Very Excellent	Very Excellent	Very Excellent	Cannot tested	Cannot tested	Cannot tested	*2

*1 Examined by making three-sided fin seal bags using
the central roll 34 of Figure 30 where both ends of
the web were slitted and heat fused.

*2 50 sheets of photographic films were covered by a
V-shaped pad made of paper board, and put in the
above three-sided fin seal bag. The opening of the
bag was sealed, and put in a fitting type decorated
box. 10 boxes of the decorated box were put in a
corrugated board box, and ^ashaking test was
conducted according to JIS Z-0322. Pinholes were
inspected by visual observation.

Example 11

A laminated film, the inner surface of which was joined by blocking with strongly joined portions and weakly joined portions, illustrated in Figures 2 and 18, was prepared from a coextruded double layer inflation film.

The outer layer was an ethylene- α -olefin copolymer resin layer composed of 70 wt. % of an ethylene-octene-1 copolymer resin having a MI of 2.0 g/10 minutes, a density of 0.918 g/cm³ and a Vicat softening point of 109°C, 26.6 wt. % of an ethylene-4-methylpentene-1 copolymer resin having a MI of 2.1 g/10 minutes, a density of 0.940 g/cm³ and a Vicat softening point of 127°C, 3 wt. % of BaSO₄, 0.3 wt. % of dimethylpolysiloxane having a viscosity of 1000 cm²/s (10,000 centi stokes) and 0.1 wt. % of 5,8-dimethyl-tocotrienol, 0.3 wt. % of calcium stearate and 0.1 wt. % of 2,6-di-*t*-butyl-paracresol, and had a thickness of 20 μ m.

The inner layer was a low softening point ethylene-butene-1 resin layer composed of 80 wt. % of an ethylene-butene-1 copolymer resin having a MI of 1.8 g/10 minutes, a density of 0.907 g/cm³ and a Vicat softening point of 86°C, 10 wt. % of a graft-modified resin of an unsaturated carboxylic acid and an EVA resin ("Adhesive EVA Resin MODIC E-200 H", tradename) having a MI of 2.5 g/10 minutes, a density of 0.94 g/cm³ and a Vicat softening point of 66°C, 0.5 wt. % of glycerine monostearate, 2 wt. % of carbon black, 0.2 wt. % of 5,8-dimethyl-tocotrienol and 7.3 wt. % of low molecular weight polyethylene wax, and had a thickness of 10 μ m.

The outer layer of the above coextruded double layer inflation film of 30 μ m in thickness was cooled by air-cooling blown from an air ring, and the inner layer was weakly joined by blocking by passing a nip roll. Then, the laminated film joined weakly by blocking was passed through a pressing apparatus composed of a metal embossing roll having longitudinal ribs 30 μ m in height 5 mm in width at 3 mm intervals heated at 80°C and a silicone rubber pressure roll which is a heat-resistant elastic roll to obtain a laminated film of 60 μ m in thickness joined by blocking with strongly joined longitudinal streaks having a four layer construction.

The laminated film was excellent in physical strength, particularly tear strength and Gelbo test strength, heat sealing properties, such as heat sealing strength, hot tack properties, sealability with other materials, heat seal strength with time and low temperature heat seal strength with time, X-ray shielding ability, antistatic ability and film moldability. Separation problems between the inner layers occurring in the lamination process to other flexible sheet and in the bag-making process resulting in the occurrence of wrinkling, streaks and blistering could be prevented without using an adhesive. Since the production of the laminated film was conducted in the coextruded double layer inflation film molding process, a plurality of laminated multilayer rolls could be produced by slitting the laminated film into the width of use by the inexpensive slitting method using the heated razor blade heated by electric resistance to around the Vicat softening point without the occurrence of e.g. separation, wrinkling, streaks or blistering (Figure 34). Light-shielding laminated multilayer films having the light-shielding ability equal to the conventional laminated films could be produced by using a

combination of 5,8-dimethyl-tocotrienol having antioxidation properties and an effect on the improvement of the light-shielding ability and dimethylpolysiloxane the viscosity of which was 1000 cm²/s (10,000 centi stokes) having an effect on the improvement of the film moldability, resin fluidity, antiblocking and light-shielding ability due to the increase of haze, even though the amount of the light-shielding material was decreased by 30 %. As a result, various unexpected results were obtained, such as the improvement in heat sealing properties, physical strength, dustproofness, appearance (the decrease of the production of insoluble lumps) and slipping characteristics. By blending glycerine monostearate as an antistatic agent into the inner layer, electrification of the laminated multilayer film composed of thermoplastic resin layers alone was prevented, and moreover, for example the degradation of the heat sealing properties and the development inhibition by the adhesion of white powder onto the photosensitive layer of photographic photosensitive materials due to the bleeding out of additives was also prevented.

Example 12

A laminated film, the inner surface of which was joined by blocking with strongly joined portions and weakly joined portions, illustrated in Figure 20 and similar to Figure 8 was prepared from a coextruded triple layer inflation film.

The outer layer was a nylon 6 resin layer of 10 μ m in thickness composed of the polyamide resin alone.

The middle layer was a modified L-LDPE resin layer of 5 μ m in thickness composed of a L-LDPE type adhesive resin modified by graft polymerization of an unsaturated carboxylic acid ("Admer NF 300", tradename) having a MI of 1.3 g/10 minutes, a density of 0.94 g/cm³ and a Vicat softening point of 100°C containing 3 wt. % of carbon black.

The inner layer was a light-shielding polyolefin resin layer of 25 μ m in thickness composed of 60 wt. % of an ethylene-butene-1 copolymer resin having a MI of 1.2 g/10 minutes, a density of 0.893 g/cm³ and a Vicat softening point of 83°C, 35 wt. % of a high pressure branched low density homopolyethylene (LDPE) resin having a MI of 5.6 g/10 minutes, a density of 0.918 g/cm³ and a Vicat softening point of 87°C, 4.5 wt. % of carbon black, 0.3 wt. % of zinc stearate and 0.2 wt. % of a phenol antioxidant ("Irganox 1010", tradename).

The inner surface of the above coextruded triple layer inflation film of 40 μ m in thickness was joined weakly by blocking by passing a nip roll, and then strongly joined lateral streaks were formed by passing a pressing apparatus with an embossing roll to obtain a laminated film of 80 μ m in thickness with strongly joined portions having a six layer construction.

A heat sealing layer of 30 μ m in thickness was provided on one side of the laminated film by directly coating the resin composition composed of 60 wt. % of a LDPE resin having a MI of 5.1 g/10 minutes and a density of 0.919 g/cm³, 27 wt. % of an ethylene-butene-1 copolymer resin having a MI of 1.2 g/10 minutes and a density of 0.920 g/cm³, 10 wt. % of an unsaturated carboxylic acid-modified L-LDPE resin ("Admer NB 050", tradename) having a MI of 3.5 g/10 minutes and a density of 0.93 g/cm³ and 3 wt. % of carbon black by the extrusion laminating method at the resin temperature of 310°C.

Example 13

The coextruded triple layer inflation film having the same thickness and resin composition as in Example 12 was used. Longitudinal ribs were formed on the inner surface of the inflation film by using a stainless steel cooling apparatus for keeping film width cooled by water at 20°C, on the surface of which longitudinal ribs were formed at 2.5 mm intervals, while the outer layer of the inflation film was air-cooled. Then, the inner surface was joined at 10 mm intervals by an embossing pressing apparatus having lateral ribs.

On the laminated film of 80 μ m in thickness having a six layer construction, a heat sealing layer of 30 μ m in thickness having the same resin composition as in Example 12 was coated by the same method.

The inner layer of the laminated film thus obtained had ribs in the longitudinal direction, and the outer layer had ribs in the lateral direction, in total having a lattice structure. The laminated film was excellent e.g. in physical strength, resistance to pinholes, Gelbo test strength and wear resistance of the outer layer, and the costs were sharply reduced. This laminated film was particularly suitable as a light-shielding bag for photographic photosensitive materials.

Particularly, the laminated films of Examples 12 and 13 are suitable as light-shielding bags for packaging heavy photographic photosensitive materials in a form of a roll or sheets having sharp edges, which is excellent in physical strength, resistance to pinholes, oxygen barrier, heat sealing properties, and low costs.

Example 14

A laminated film wherein the end portions were joined more strongly than the central portion was prepared. The layer construction corresponds to Figure 22.

A single layer inflation film of 50 μ m in thickness and 150 cm in lay-flat width was molded from the polyolefin resin composition composed of 40 wt. % of an ethylene-4-methylpentene-1 copolymer resin having a MI of 2.0 g/10 minutes and a density of 0.930 g/cm³, 20 wt. % of an ethylene-butene-1 copolymer resin having a MI of 1.2 g/10 minutes and a

density of 0.90 g/cm³, 26.8 wt. % of a LDPE resin having a MI of 5.4 g/10 minutes and a density of 0.918 g/cm³, 10 wt. % of an acid-modified L-LDPE resin, 0.2 wt. % of a dibenzilidenesorbitol organic nucleating agent and 3 wt. % of carbon black coated with calcium stearate, using an inflation film molding machine at the resin temperature of 190°C at the blow-up ratio of 1.2. After air-cooling, the inner layer of the inflation film was weakly joined over the whole surface by blocking by heating using an infrared heater immediately before a nip roll and by passing the nip roll so that the peeling strength was 3 g/15 mm width. Then, using the apparatus shown in Figure 34, the inflation film was provided with two strongly joined lines 30 mm in width with an oblique lattice pattern by passing the embossing rolls heated at 120°C so that the peeling strength was 550 g/15 mm width, and the strongly joined portions were slitted by the heated razor blade at 90°C into three webs of 50 cm in width.

Example 15

A laminated film corresponding to Figure 25 was prepared.

The outer layer was 25 µm in thickness and composed of 40 wt. % of an ethylene-octene-1 copolymer resin having a MI of 2.1 g/10 minutes and a density of 0.920 g/cm³, 40 wt. % of an ethylene-4-methylpentene-1 copolymer resin having a MI of 3.1 g/10 minutes and a density of 0.940 g/cm³, 10 wt. % of an acid-modified ethylene-4-methylpentene-1 copolymer resin, 3 wt. % of oil furnace carbon black, the surface of which was treated with erucic amide and 0.05 wt. % of a phenol antioxidant.

The inner layer of 25 µm in thickness was composed of the same resin composition as in Example 14 except that an EVA resin was used instead of the LDPE resin.

The coextruded double layer inflation film composed of the above outer and inner layers of 180 cm in lay-flat width was molded using an inflation film molding machine at the outer layer resin temperature of 200°C and the inner layer resin temperature of 180°C at the blow-up ratio of 1.5. After air-cooling, the inner layer of the inflation film was weakly joined over the whole surface by blocking by passing the nip roll so that the peeling strength was 12 g/15 mm width. Then, using the apparatus shown in Figure 34, the inflation film was provided with two strongly joined lines 30 mm in width with an oblique lattice pattern by passing the embossing rolls heated at 80°C so that the peeling strength was 75 g/15 mm width, and the strongly joined portions were slitted by the heated razor blade at 100°C into three webs of 60 cm in width.

Example 16

A laminated film corresponding to Figure 27 was prepared.

An aluminum (40nm [400 Å]) metallized biaxially stretched polyester resin film of 12 µm in thickness was laminated onto the laminated film of Example 15 through an adhesive layer of 15 µm in thickness composed of 60 wt. % of a LDPE resin and 40 wt. % of an ethylene-butene-1 copolymer resin provided by extrusion laminating at the resin temperature of 320°C.

Light-shielding bags made of the laminated film were excellent e.g. in sealability, light-shielding ability, physical strength, moistureproofness, gas barrier, resistance to pinholes, heat sealing properties, such as heat sealing strength, hot tack properties, heat seal strength with time and appearance.

Example 17

The coextruded double layer inflation film used was 70 µm in thickness, 120 cm in lay-flat width and composed of an outer layer of 20 µm in thickness composed of 20 wt. % of a homopolyethylene resin having a MI of 2.1 g/10 minutes, a density of 0.960 g/cm³ and a softening point of 128°C, 72.75 wt. % of an ethylene-octene-1 copolymer resin having a MI of 1.5 g/10 minutes, a density of 0.920 g/cm³ and a Vicat softening point of 103°C, 6 wt. % of titanium dioxide in anatase form, the surface of which was treated with water-containing aluminum oxide, 0.05 wt. % of a phenol antioxidant and 0.2 wt. % of a dibenzilidenesorbitol compound, and an inner layer of 15 µm in thickness composed of 70 wt. % of an ethylene-butene-1 copolymer resin having a MI of 2.0 g/10 minutes, a density of 0.90 g/cm³ and a Vicat softening point of 83°C and 30 wt. % of a LDPE resin having a MI of 3.8 g/10 minutes, a density of 0.920 g/cm³ and a Vicat softening point of 89°C. The inner layer of the inflation film was weakly joined over the whole surface by blocking by passing the nip roll so that the peeling strength was 15 g/15 mm width. The central portion of the laminated film was strongly joined by blocking 2 cm in width by passing a heating pressure roll at 80°C so that the peeling strength was 93 g/15 mm width, and the strongly joined portion was slitted by a heated razor blade at 100°C into two webs of 60 cm in width. A polyvinylidene chloride-coated biaxially stretched polypropylene resin film with printing was laminated onto the above laminated film through an extrusion laminated adhesive layer of 15 µm in thickness composed of a LDPE resin containing 15 wt. % of an acid-modified LDPE resin so that the printed side faced the laminated film.

Example 18

The inflation film used was a polyolefin resin film of 50 μm in thickness containing carbon black and was composed of 5 wt. % of a homopolyethylene resin having a MI of 1.1 g/10 minutes and a density of 0.954 g/cm³, 87 wt. % of an ethylene-4-methylpentene-1 copolymer resin having a MI of 2.1 g/10 minutes and a density of 0.920 g/cm³, 4.5 wt. % of a LDPE resin having a MI of 2.4 g/10 minutes and a density of 0.923 g/cm³, 3 wt. % of oil furnace carbon black having a mean particle size of 21nm (μm), 0.05 wt. % of erucic amide and 0.1 wt. % of antioxidant, and the softening point was 102°C. The inflation film was deflated by passing a nip roll, and both edges were slitted by using the cutting apparatus shown in Figure 35. The razor blade was heated to 88°C, and the winding speed of each roll was adjusted to 30 m/min. Since both blades were heated as the whole, locational temperature elevation by friction of the film was inhibited, and the film was softened. As a result, the sharpness of the blade was kept after continuous slitting for 240 hours. Then, a further film could be slitted without changing the blade. The cut end portion was melted by the heat of the blade, and cuttings and carbon powder adhered to the melted cut end portion. Therefore, the scattering of cuttings and carbon powder were very small. Since the cut end was thickened, the tear strength in the longitudinal direction was 807 g and that in the lateral direction was 1,040 g. As a result, film rupture did not occur through the film molding process and the laminating process for laminating other flexible sheets. On the other hand, when the blades were used without heating at 25°C, the sharpness of the blades was degraded, and it was necessary to change them after continuous cutting for 38 hours.

Example 19

The inflation film used was a polyolefin resin film of 100 μm in thickness containing carbon black, and was composed of 96.8 wt. % of a LDPE resin having a MI of 3.2 g/10 minutes and a density of 0.922 g/cm³, 3 wt. % of oil furnace carbon black having a mean particle size of 21nm (μm), 0.05 wt. % of oleic amide, 0.1 wt. % of a phenol antioxidant, 0.05 wt. % of zinc stearate and 0.05 wt. % of synthetic silica, and the softening point was 92°C. The inflation film was deflated by passing a nip roll, and both edges were slitted by using the cutting apparatus shown in Figure 35. The razor blade was heated to 77°C and the winding speed of each roll was adjusted to 25 m/min. As a result, the sharpness of the blade was kept after continuous slitting for 240 hours. Since the cut end portion was melted by the heat of blade, the scattering of cuttings and carbon powder were very small. The cut end was thickened, and the tear strength in the longitudinal direction was 211 g and that in the lateral direction was 895 g. As a result, film rupture did not occur through the film molding process and the laminating process for laminating other flexible sheets. On the other hand, when the blades were used without heating, the sharpness of the blades was degraded, and it was necessary to change them after continuous cutting for 68 hours.

Example 20

The inflation film used was a coextruded double layer inflation film, the outer layer of which was 25 μm in thickness. It was composed of 76.6 wt. % of an ethylene-4-methylpentene-1 copolymer resin having a MI of 2.1 g/10 minutes and a density of 0.920 g/cm³, 20 wt. % of a homopolyethylene resin having a MI of 1.1 g/10 minutes, a density of 0.954 g/cm³ and a Vicat softening point of 126°C, 3 wt. % of oil furnace carbon black having a mean particle size of 21nm (μm), 0.1 wt. % of oleic amide, 0.2 wt. % of calcium stearate and 0.1 wt. % of an antioxidant, and had a softening point of 113°C. The inner layer of 25 μm in thickness was composed of 92.4 wt. % of an ethylene-4-methylpentene-1 copolymer resin having a MI of 2.0 g/10 minutes and a density of 0.920 g/cm³, 4.5 wt. % of a LDPE resin having a MI of 2.4 g/10 minutes and a density of 0.923 g/cm³, 3 wt. % of oil furnace carbon black and 0.1 wt. % of an antioxidant, and had a softening point of 98°C.

The inflation film was deflated, and the inner layer was joined by blocking. The lay-flat width was 1,500 mm, and the thickness was 100 μm . The inflation film was slitted into three webs by using the cutting apparatus of Figure 30. The razor blade was heated to 98°C, and the winding speed of each roll was adjusted to 15 m/min. As a result, both blades kept sharpness after continuous slitting for 240 hours, and a further film could be slitted without changing the blade. The cut end portion was melted by the heat of blade and cuttings did not generate. The cut end portion was thickened, and both of the tear strength in the longitudinal direction and that in the lateral direction were more than 1,600 g. The cut end portions were melted and formed heat fused portions, and the slitted laminated films had the aforementioned superiorities of the laminated film joined by blocking, wherein the cut end portion forms a heat fused portion. On the other hand, when the blades were used without heating at 25°C, the sharpness of the blades was degraded, and it was necessary to change them after continuous cutting for 26 hours.

Example 21

The inflation film used was a coextruded double layer inflation film, the outer layer of which was 25 μm in thickness.

It was composed of 76.6 wt. % of an ethylene-4-methylpentene-1 copolymer resin having a MI of 2.1 g/10 minutes, a density of 0.920 g/cm³ and a Vicat softening point of 100°C, 20 wt. % of a HDPE resin having a MI of 1.1 g/10 minutes, a density of 0.954 g/cm³ and a Vicat softening point of 126°C, 3 wt. % of oil furnace carbon black having a mean particle size of 21nm (μm), 0.05 wt. % of oleic amide, 0.1 wt. % of an antistatic agent and 0.05 wt. % of an antioxidant, and had a Vicat softening point of 108°C. The inner layer of 25 μm in thickness was composed of 70 wt. % of an ethylene-4-methylpentene-1 copolymer resin having a MI of 2.0 g/10 minutes, a density of 0.922 g/cm³ and a Vicat softening point of 102°C and 4.5 wt. % of a very low density polyethylene resin having a MI of 1.2 g/10 minutes, a density of 0.892 g/cm³ and a Vicat softening point of 76°C. The inner layer was joined by blocking by heating by an inflation heater provided before a nip roll and pressing by the nip roll so that the peeling strength was 5 g/15 mm width. The inflation film of 100 μm in thickness was slitted into three webs by using the cutting apparatus of Figure 30. The razor blade was heated to 102°C, and the winding speed of each roll was adjusted to 15 m/min. As a result, both blades kept sharpness after continuous slitting for 200 hours. The cut end portion was melted by the heat of blade and cuttings did not generate. The cut end portion was thickened, and both of the tear strength in the longitudinal direction and that in the lateral direction were more than 1,600 g. The peeling strength of the cut end portions was 8 g/15 mm width and 7.5 g/15 mm width, respectively, which were greater than the other parts, the peeling strength of which was 5 g/15 mm width. The laminated film did not separate from the cut end portion through the film forming process and the laminating process. On the other hand, when the blades were used without heating at 25°C, the sharpness of the blades was degraded, and they were necessary to be changed after continuous cutting for 22 hours. By providing the ion sputter, the electric potential of the film reduced to less than 50 V, less than one third of the film not provided with the ion sputter. The electric shock was not observed at touching the film by hand. The adhesion of dust and cutting were rarely observed.

In the case of slitting a laminated film of 100 μm in thickness was obtained composed of a coextruded double layer inflation film made of an ethylene- α -olefin copolymer resin containing carbon black, the inner layer of which was joined by blocking which had a very great tear strength of more than 1,600 g in the longitudinal direction, the continuous slitting time was 240 hours by using the heated razor blade at about 100°C. When the blade was not heated, the continuous slitting time was 26 hours.

In the case of slitting a polyolefin resin film containing carbon black having a tear strength particularly in the longitudinal direction smaller than the above coextruded double layer inflation film of ethylene- α -olefin copolymer resin, such as a film of a LDPE resin having a MI of 2.4 g/10 minutes and a density of 0.924 g/cm³ containing 3 wt. % of carbon black, the tear strength of which in the longitudinal direction was 53 g less than 1/30, the continuous slitting could be more than 360 hours.

The resins suitable for the slitting by the heated razor blade are various thermoplastic resin films, such as polyolefin resin films, polyamide resin films, cellulose triacetate films, polystyrene resin films, synthetic papers and polycarbonate resin films, and the slittable life can be lengthened.

Claims

1. A laminated film comprising two thermoplastic resin films, the inner surfaces of which are joined by blocking, said film having strongly joined portions and weakly joined portions, wherein the peeling strength of the strongly joined portions is at least twice that of the weakly joined portions.
2. The laminated film of claim 1, wherein the laminated film is made of a deflated inflation film.
3. The laminated film of claim 1 or 2, which contains a light-shielding material in at least two layers.
4. The laminated film of any of claims 1 to 3, wherein the end portions are joined more strongly than the central portion.
5. The laminated film of claim 4, wherein the strongly joined portions are cut ends joined by heat fusion.
6. The laminated film of claim 5, wherein the inflation film comprises an outer layer and an inner layer having a softening point lower than the outer layer.
7. The laminated film of claim 1, wherein the thermoplastic resin film is a coextruded multilayer inflation film, the inner surface of which is joined by blocking, wherein the Shore hardness of the inner layer comprising the thermoplastic resin is lower than that of the outer layer comprising the thermoplastic resin.
8. The laminated film of claim 1, wherein the thermoplastic resin film is a coextruded multilayer inflation film, the inner surface of which is joined by blocking, wherein the inner layer comprises an acid-modified polyolefin resin.

9. The laminated film of any of claims 5 to 8, wherein the outer layer has a Vicat softening point higher than the inner layer, and heat sealability.
- 5 10. The laminated film of any of claims 5 to 8, wherein a heat-resistant flexible sheet having a Young's modulus of not less than 50 kg/mm² is laminated directly or through an adhesive layer.
11. The laminated film of any of claims 5 to 8, wherein a heat sealing layer having a Vicat softening point lower than the outer layer is laminated directly or through an adhesive layer.
- 10 12. A process of producing a laminated film of any of claims 1 to 11 which comprises
pressing two thermoplastic resin films by an embossing roll or
flat-pressing a tubular film molded by an inflation process, by a pressure roll into flat to join the inner surfaces
15 by blocking, and cutting by fusion.
13. The process of claim 12, wherein the thermoplastic resin films are heated prior to the pressing.
14. The process of claim 12, wherein the embossing roll is a pressure roll having ribs at constant intervals in the lateral
20 direction.
15. The process of claim 12, wherein the surface of the tubular film is heated prior to the pressing by a pressure roll.
16. The process of claim 12, wherein the cutting by fusion is effected by a razor blade heated to a temperature ranging
25 from 50°C to the melting point of the film.
17. The process of claim 16, wherein the cut end of the film is thickened.

Patentansprüche

- 30 1. Eine Verbundfolie, die zwei thermoplastische Harzfolien enthält, wobei ihre Innenflächen durch Verblocken miteinander verbunden sind, wobei die Folie fest verbundene Bereiche und nur schwach verbundene Bereiche aufweist, wobei die Haftfestigkeit der stark verbundenen Bereiche mindestens doppelt so groß ist wie die der schwach verbundenen Bereiche.
- 35 2. Verbundfolie gemäß Anspruch 1, worin die Verbundfolie aus einer abgeflachten Blasfolie hergestellt wird.
3. Verbundfolie gemäß Anspruch 1 oder 2, die ein Lichtschutz-Material in mindestens zwei Schichten enthält.
- 40 4. Verbundfolie gemäß einem oder mehreren der Ansprüche 1, 2 oder 3, bei der die Endbereiche stärker miteinander verbunden sind als der Zentrale Bereich.
5. Verbundfolie gemäß Anspruch 4, bei der die fest verbundenen Bereiche Schnittenden sind, die durch Wärmever-
schmelzung miteinander verbunden sind.
- 45 6. Verbundfolie gemäß Anspruch 5, worin die Blasfolie eine äußere Schicht und eine innere Schicht enthält, die einen niedrigeren Erweichungspunkt aufweist als die äußere Schicht.
7. Verbundfolie gemäß Anspruch 1, worin die thermoplastische Harzschicht eine coextrudierte, vielschichtige Blasfo-
50 lie ist, deren innere Oberfläche durch Verblocken verbunden ist, wobei die Shore-Härte der inneren Schicht, die das thermoplastische Harz enthält, geringer ist als die der äußeren Schicht, die das thermoplastische Harz enthält.
8. Verbundfolie gemäß Anspruch 1, wobei die thermoplastische Harzfolie eine coextrudierte, vielschichtige Blasfolie ist, deren innere Oberfläche durch Verblocken verbunden ist, wobei die innere Schicht ein Säure-modifiziertes
55 Polyolefinharz enthält.
9. Verbundfolie gemäß einem der Ansprüche 5 bis 8, wobei die äußere Schicht einen Vicat-Erweichungspunkt aufweist, der höher ist als der der inneren Schicht und eine Heißsiegelfähigkeit.

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10. Verbundfolie gemäß einem oder mehreren der Ansprüche 5 bis 8, wobei ein wärmeresistentes, flexibles Blatt mit einem Young'schen Modul von nicht weniger als 50 kg/mm² direkt oder über eine Haftschrift laminiert wird.

11. Verbundfolie gemäß einem oder mehreren der Ansprüche 5 bis 8, worin eine Heißsiegel-Schicht mit einem Vicat-Erweichungspunkt, der geringer ist als der der äußeren Schicht direkt oder über eine Haftschrift laminiert wird.

12. Verfahren zur Herstellung einer Verbundfolie gemäß einem oder mehreren der Ansprüche 1 bis 11, das folgende Schritte enthält:

Pressen von zwei thermoplastischen Harzschichten durch eine Prägerolle oder

Flachpressen von einer röhrenförmigen Folie, die durch ein Blasverfahren geformt wurde durch eine Preßrolle in den flachen Zustand, um die inneren Oberflächen durch Verblocken zu verbinden und Schneiden durch Wärmeinwirkung.

13. Verfahren gemäß Anspruch 12, wobei die thermoplastischen Harzfolien vor dem Pressen erhitzt werden.

14. Verfahren gemäß Anspruch 12, wobei die Prägewalze eine Preßwalze ist, die in konstanten Abständen in seitlicher Richtung Rippen aufweist.

15. Verfahren gemäß Anspruch 12, wobei die Oberfläche der röhrenförmigen Folie erhitzt wird, bevor sie durch die Preßwalze gepreßt wird.

16. Verfahren gemäß Anspruch 12, wobei das Schneiden durch Wärmeinwirkung durch eine Rasierklinge durchgeführt wird, die auf eine Temperatur erhitzt wird, die zwischen 50°C und dem Schmelzpunkt der Folie liegt.

17. Verfahren gemäß Anspruch 16, wobei das Schnittende der Folie eingedickt wird.

Revendications

1. Film stratifié comprenant deux films de résine thermoplastique dont les surfaces internes ont été jointes par adhérence de contact, ledit film possédant des portions fortement jointes et des portions faiblement jointes, dans lequel la résistance au décollement des portions fortement jointes représente au moins le double de celle des portions faiblement jointes.

2. Film stratifié selon la revendication 1, dans lequel le film stratifié est réalisé à partir d'un film obtenu par gonflage et qui a été dégonflé.

3. Film stratifié selon la revendication 1 ou 2, qui contient une matière de protection contre l'effet de la lumière dans au moins deux couches.

4. Film stratifié selon l'une quelconque des revendications 1 à 3, dans lequel les portions terminales sont jointes plus fortement que la portion centrale.

5. Film stratifié selon la revendication 4, dans lequel les portions fortement jointes sont des extrémités découpées jointes par thermofusion.

6. Film stratifié selon la revendication 5, dans lequel le film obtenu par gonflage comprend une couche externe et une couche interne qui possède un point de ramollissement inférieur à celui de la couche externe.

7. Film stratifié selon la revendication 1, dans lequel le film de résine thermoplastique est un film multicouche coextrudé obtenu par gonflage, dont la surface interne est jointe par adhérence de contact, dans lequel la dureté Shore de la couche interne comprenant la résine thermoplastique est inférieure à celle de la couche externe comprenant la résine thermoplastique.

8. Film stratifié selon la revendication 1, dans lequel le film de résine thermoplastique est un film multicouche coextrudé obtenu par gonflage, dont la surface interne est jointe par adhérence de contact, dans lequel la couche interne comprend une résine de polyoléfine modifiée par un acide.

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9. Film stratifié selon l'une quelconque des revendications 5 à 8, dans lequel la couche externe possède un point de ramollissement de Vicat supérieur à celui de la couche interne, ainsi qu'une aptitude au thermosoudage.
- 5 10. Film stratifié selon l'une quelconque des revendications 5 à 8, dans lequel on stratifie une feuille flexible thermorésistante possédant un module de Young qui n'est pas inférieur à 50 kg/mm², directement ou via une couche adhésive.
- 10 11. Film stratifié selon l'une quelconque des revendications 5 à 8, dans lequel on stratifie une couche de thermoscelage dont le point de ramollissement de Vicat est inférieur à celui de la couche externe, directement ou via une couche adhésive.
12. Procédé pour préparer un film stratifié selon l'une quelconque des revendications 1 à 11, qui comprend le fait de
- 15 presser deux films de résine thermoplastique à l'aide d'un rouleau d'estampage ou
- presser à plat un film tubulaire moulé à l'aide d'un processus de gonflage, en utilisant un rouleau presseur pour joindre à plat les surfaces internes par adhérence de contact, et découper par fusion.
- 20 13. Procédé selon la revendication 12, dans lequel les films de résine thermoplastique sont chauffés avant d'être pressés.
14. Procédé selon la revendication 12, dans lequel le rouleau d'estampage est un rouleau presseur comportant des nervures à intervalles réguliers en direction latérale.
- 25 15. Procédé selon la revendication 12, dans lequel la surface du film tubulaire est chauffée avant d'être pressée par un rouleau presseur.
16. Procédé selon la revendication 12, dans lequel le découpage par fusion est réalisé à l'aide d'une lame de rasoir chauffée à une température se situant dans le domaine allant de 50°C au point de fusion du film.
- 30 17. Procédé selon la revendication 16, dans lequel l'extrémité découpée du film est épaisse.

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FIG. 1

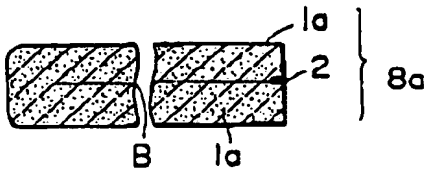


FIG. 4

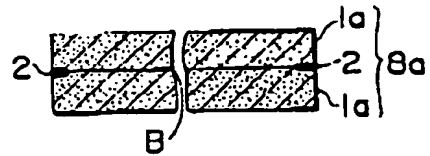


FIG. 2

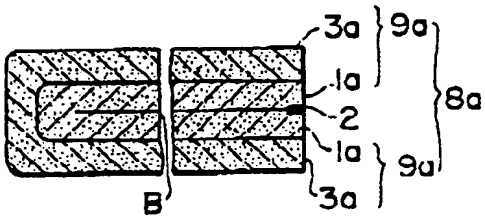


FIG. 5

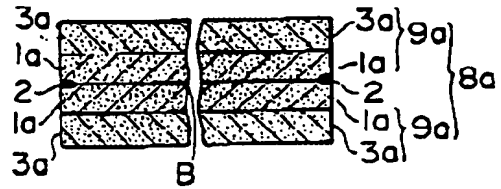


FIG. 3

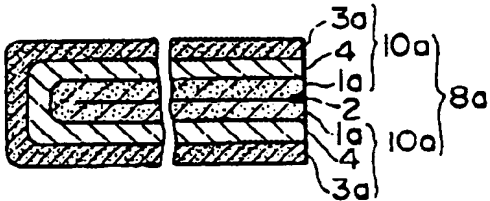


FIG. 6

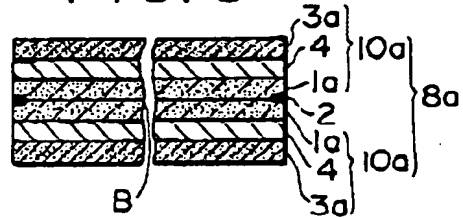


FIG. 7

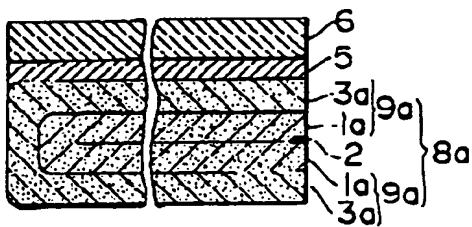


FIG. 8

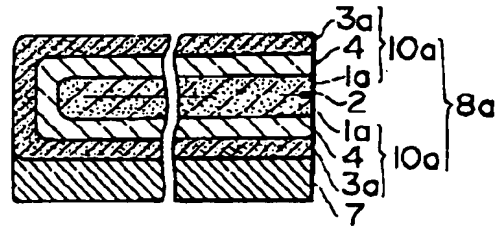


FIG. 9

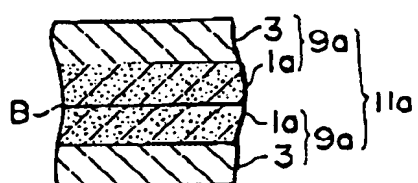


FIG. 10

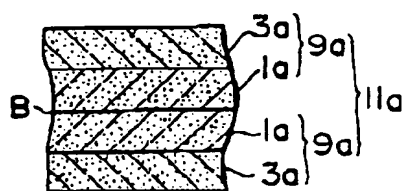


FIG. 11

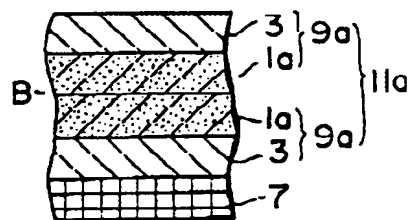


FIG. 12

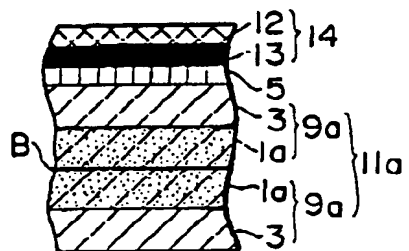


FIG. 13

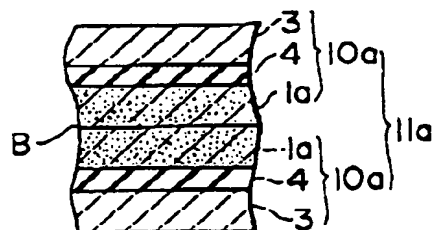


FIG. 14

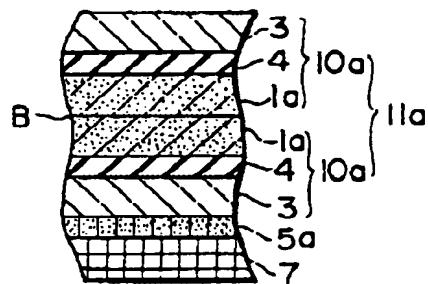


FIG. 15

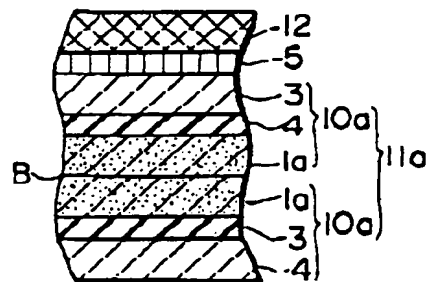


FIG. 16

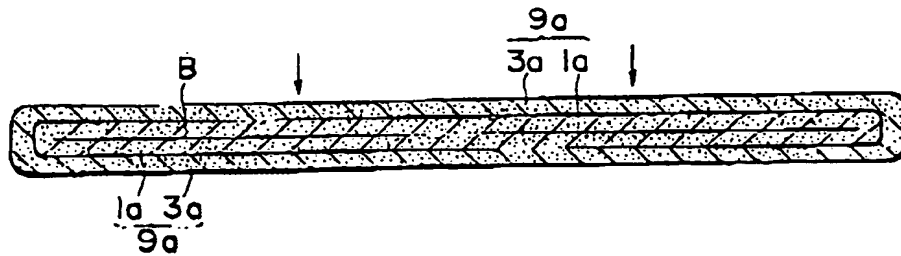


FIG. 17

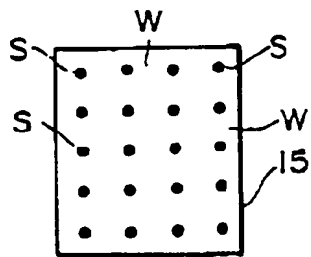


FIG. 20

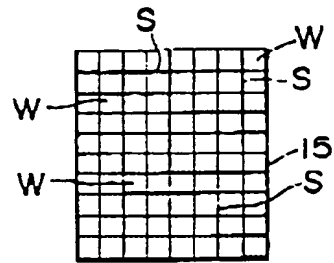


FIG. 18

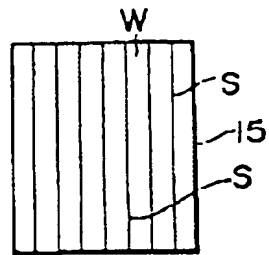


FIG. 21

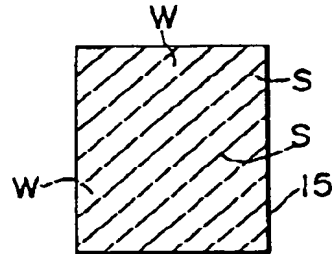


FIG. 19

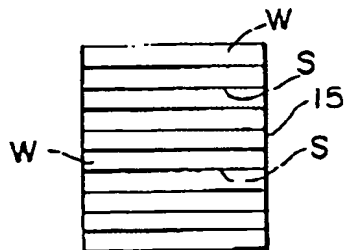


FIG. 22

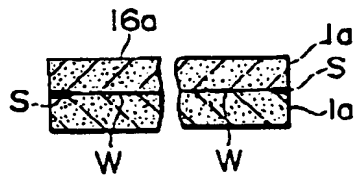


FIG. 26

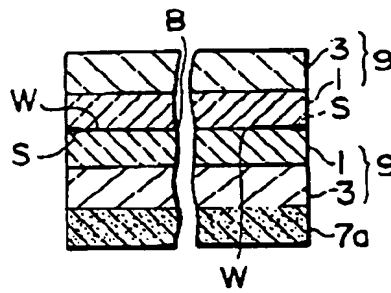


FIG. 23

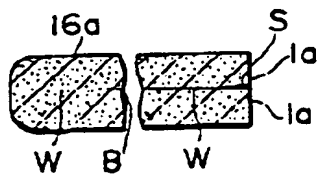


FIG. 27

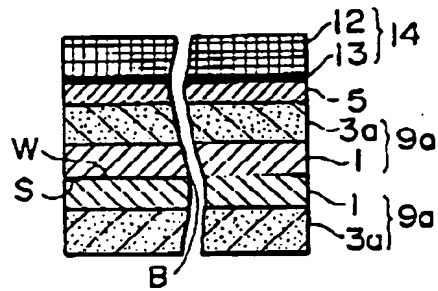


FIG. 24

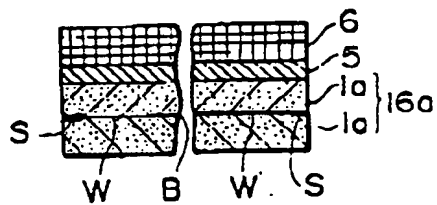


FIG. 25

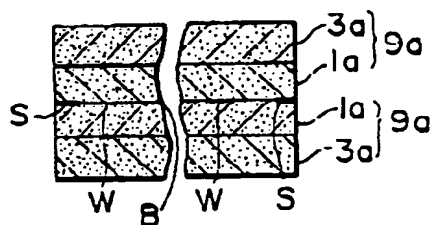


FIG. 28

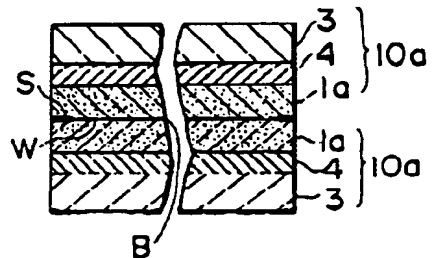


FIG. 29

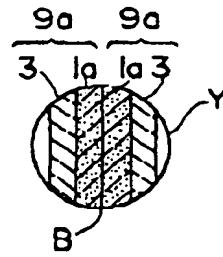
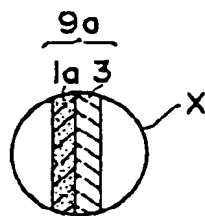
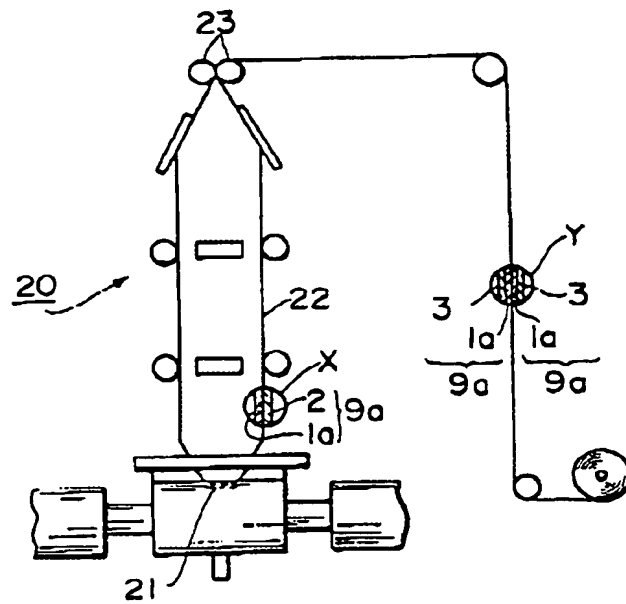


FIG. 30

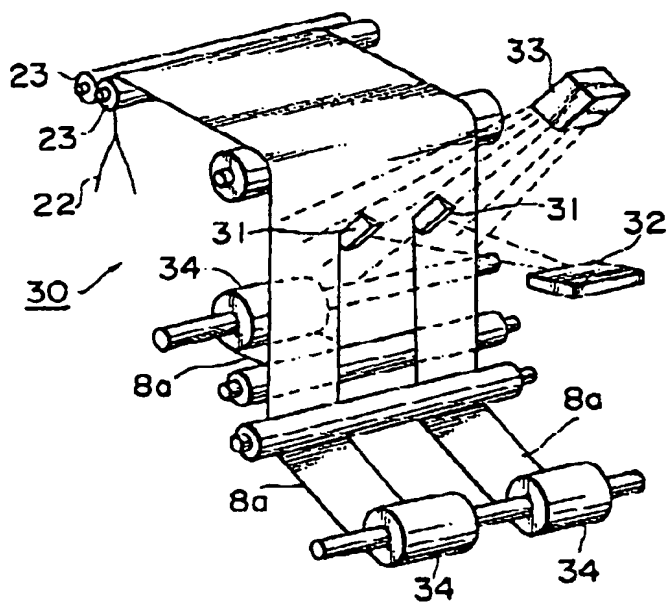


FIG. 31

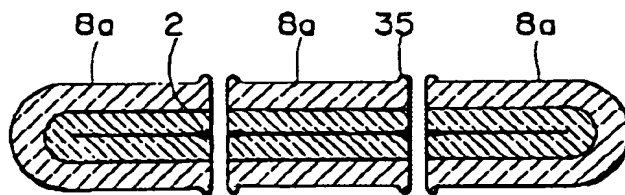


FIG. 32

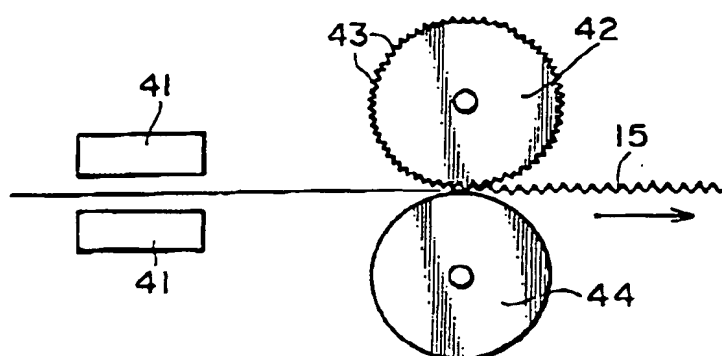


FIG. 33

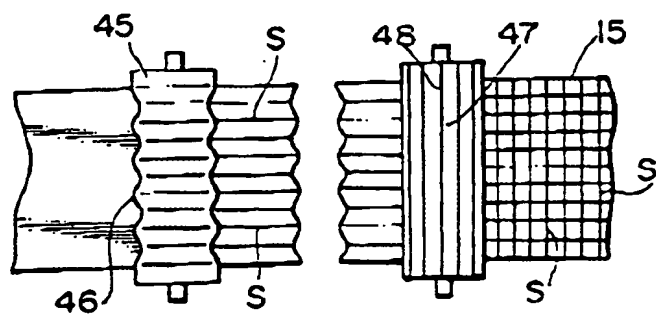


FIG. 34

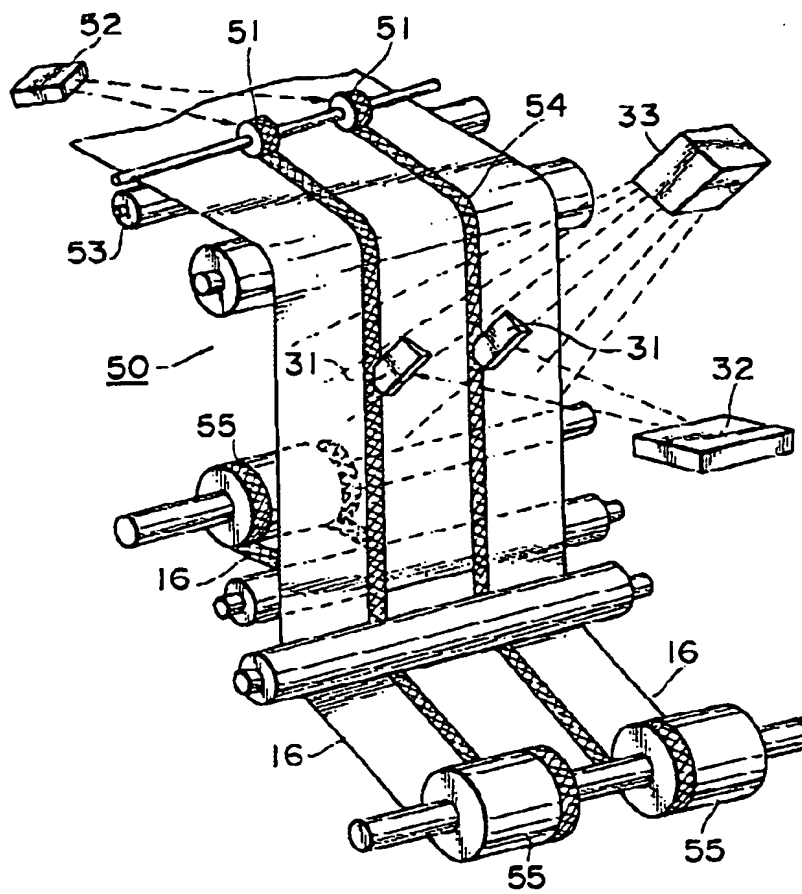


FIG. 35

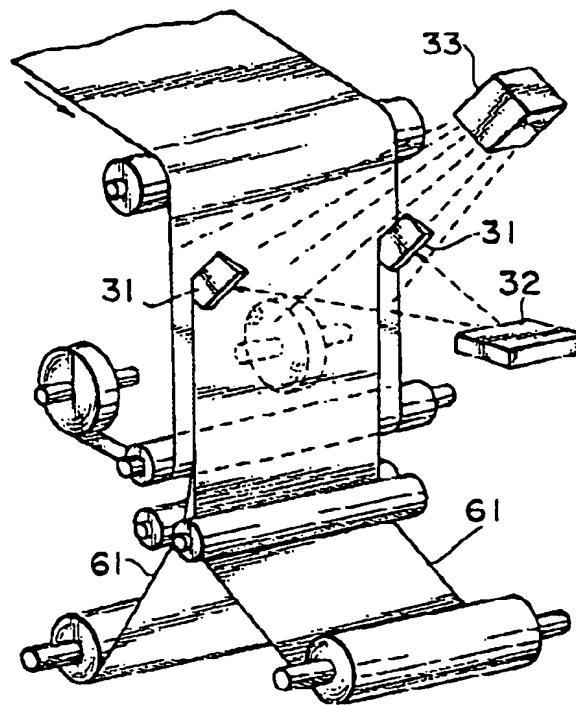


FIG. 36

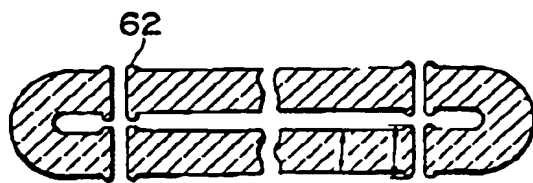
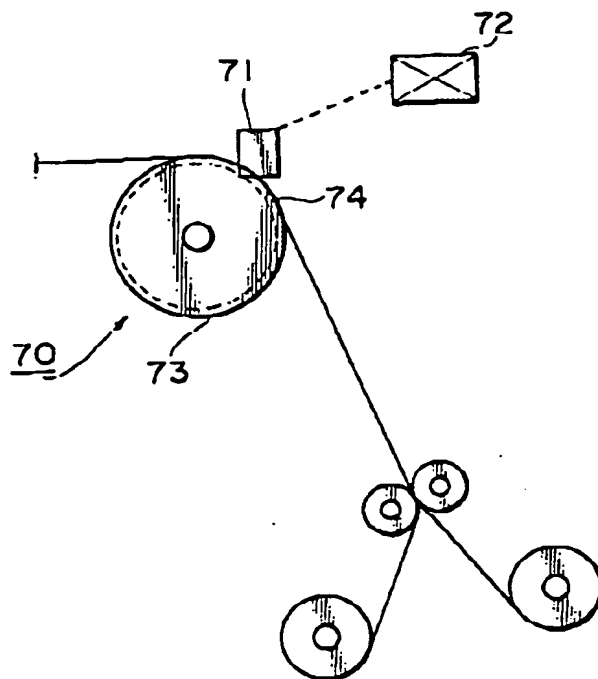


FIG. 37



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